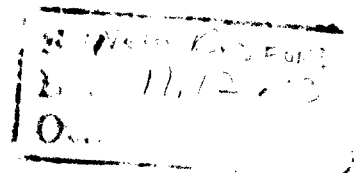




60175  
GE Corporate Research  
and Development

Research and Development Center  
General Electric Company  
P.O. Box 8, Schenectady, NY 12301  
518 387-

Building K1-3B29  
January 23, 1989



Dr. James L. Lake  
EPA, Environmental Research Laboratory  
Narragansett, RI 02882



SDMS DocID 60175

Dear Jim:

I have just been informed by Paul Galvani, counsel for Aerovox, that I should turn over to EPA several classes of documents relating to the analytical work that we did on Acushnet River sediments back in 1986, and that you could serve as the official EPA recipient of this material. The documentation requested consisted of essentially all available information relating to:

1. Sampling procedures and chain-of-custody proofs
2. Analytical protocols used
3. All analytical data
4. Computer tapes of data.

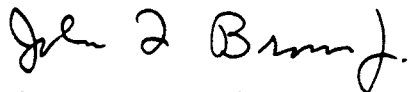
As you may recall, on November 21, 1988 I sent you a voluminous data package, which included both computer print-outs and gas chromatograms of all 24 samples that we analysed, along with a map showing the points of origin of the specimens analysed, GM-MS data, and tables that compiled and summarized our analytical results; in short, all of the available information pertinent to requests (3) and (4). In this letter I include all the data I have regarding requests (1) and (2). Regarding the latter, I could further point out that our procedures have also been described in two of our published papers (Northeast. Environ. Sci., 3:167-179, 1984; Environ. Toxicol. Chem., 6:579-593, 1987). At any event, you are now in possession of all the requested documentation, which I suppose you will have to keep on file until one of your legal colleagues asks for it.

To move from legalism to science, we have been continuing to examine the chromatograms of both biota and sediments from various sites, and continuing to turn up new PCB alteration patterns now and then. At the moment, it looks as though the Pattern H and H' dechlorination, which we found in the upper Achushnet Estuary, may also be occurring at a great many (though not all) sites in the Hudson Estuary, all the way from Troy to the Battery. Fragmentary data suggests that Newark Bay may be a different story, however, as may also be Long Island Sound, and I'd still be interested in any of your samples or chromatograms that indicated what was going on off the rest of the New England Coast.

We have also been able to duplicate a dechlorination that looks very much like Pattern H' in culture, using an anaerobic microbial growth procedure

slightly different from the one John Quensen used to bring up a dechlorination similar to upper Hudson sediment Pattern C. I suspect that someone from our group may be talking about this at our semi-annual Region 1 seminar in Boston (actually, the Cambridge Marriott this time, I think) on February 9. Unfortunately, I won't be able to be there myself, owing to long-standing arrangements for cross-country skiing in Glacier National Park that week, but my colleagues will be able to convey messages or samples.

Sincerely yours,



John F. Brown, Jr.  
Manager-Health Research  
Biological Sciences Laboratory

JFB/j

Encl.

cc: HL Finkbeiner  
PB Galvani

## ACUSHNET SEDIMENT SAMPLING FOR GE ANALYSES

### Documentation Package

#### History of GE work on Acushnet Estuary Sediments (i.e. Site and Sample Selection)

1. May, 1986. Examined collection of old gas chromatograms run by Versar in 1982-83. Found evidence of widespread but limited dechlorination.
2. May 26, 1986, Telephoned finding to Stu Richardson of Aerovox. Indicated need for new samples for high resolution capillary GC to characterize transformation. He suggested I talk to Paul Galvani, his attorney.
3. I agreed to undertake capillary GC analyses on 24 specimens--taken at two levels (2-3" and 6-7") from each of 12 sites -- 6 on each side of estuary. Samples were to be collected by GHR Analytical by walking out on mud flats at low tide, digging a hole, and taking sediments at designated depths.
4. June 9, 1986 GHR sent GE samples from 26 sites (received 6-10-86). JF Brown selected 12 pairs for detailed PCB analysis and submitted them to RE Wagner (analyst) for analysis for procedure in use in laboratory.

#### Documentation in Package

- a. Chain-of-custody forms for samples.
- b. Maps showing GHR sampling locations.
- c. JF Brown's record of sample examination and selection for analysis.
- d. GHR report on oil and grease analyses on sediments.
- e. GHR certification.

John F. Brown, Jr.  
(1-20-89)

JFB/j

GHR Analytical Inc.  
26 Main St., Lakeville, MA

CHAIN OF CUSTODY RECORD

PROJECT NO.: 29-272		WORK PLAN NO.:		SITE NAME: Upper Acushnet River Estuary		NO. OF CON- TAINERS											REMARKS
SAMPLERS (SIGNATURE): <i>Stephen O'Neil</i>																	
STATION NO.	DATE	TIME	COMP.	GRAB	STATION LOCATION												
56114	6/6/86	1335		✓	AR-1A 3 inches	1											
56115	6/6/86	1339		✓	AR-1B 7 "	1											
56116	6/6/86	1345		✓	AR-2A 3 "	1											
56117	6/6/86	1349		✓	AR-2B 7 "	1											
56118	6/6/86	1356		✓	AR-3A 3 "	1											
56119	6/6/86	1400		✓	AR-3B 7 "	1											
56120	6/6/86	1405		✓	AR-4A 3 "	1											
56121	6/6/86	1407		✓	AR-4B 7 "	1											
56122	6/6/86	1410		✓	AR-5A 3 "	1											
56123	6/6/86	1413		✓	AR-5B 7 "	1											
56124	6/6/86	1416		✓	AR-6A 3 "	1											
56125	6/6/86	1417		✓	AR-6B 7 "	1											
56126	6/6/86	1448		✓	AR-7A 3 "	1											
56127	6/6/86	1450		✓	AR-7B 7 "	1											
RELINQUISHED BY (SIGNATURE): <i>Stephen O'Neil</i>		DATE/TIME: 6/7/86 1700		RECEIVED BY (SIGNATURE): Federal Express Air Bill # 02745		RELINQUISHED BY (SIGNATURE): Federal Express Air Bill # 02745		DATE/TIME: 6/10/86 1100		RECEIVED BY (SIGNATURE): <i>Helen H. Walton</i>							
RELINQUISHED BY (SIGNATURE): <i>Helen H. Walton</i>		DATE/TIME: 6/10/86 1300		RECEIVED BY (SIGNATURE):		RELINQUISHED BY (SIGNATURE):		DATE/TIME:		RECEIVED BY (SIGNATURE):							
RELINQUISHED BY (SIGNATURE):		DATE/TIME:		RECEIVED FOR LABORATORY BY (SIGNATURE): <i>Robert E. Wagon</i>		DATE/TIME: 6/10/86 1300		REMARKS:									

GHR Analytical Inc.  
26 Main St., Lakeville, MA

CHAIN OF CUSTODY RECORD

PROJECT NO.: 29-272		WORK PLAN NO.:		SITE NAME: Upper Acushnet River Estuary		NO. OF CON- TAINERS	<div style="display: flex; justify-content: space-between;"> <div style="width: 40%; border-bottom: 1px solid black;"></div> <div style="width: 55%;">           Suffix A → Sample taken at 3 inch depth            " B → " " " 7 " "         </div> </div>									
SAMPLERS (SIGNATURE): <i>Stephen O'Neil</i>																
STATION NO.	DATE	TIME	COMP.	GRAB	STATION LOCATION											
56128	6/6/86	1453		✓	AR-8A 3 inches	1										
56129	6/6/86	1455		✓	AR-8B 7 "	1										
56130	6/6/86	1500		✓	AR-9A 3 "	1										
56131	6/6/86	1503		✓	AR-9B 7 "	1										
56132	6/6/86	1525		✓	AR-10A 3 "	1										
56133	6/6/86	1526		✓	AR-10B 7 "	1										
56134	6/6/86	1528		✓	AR-11A 3 "	1										
56135	6/6/86	1532		✓	AR-11B 7 "	1										
56136	6/6/86	1542		✓	AR-12A 3 "	1										
56137	6/6/86	1545		✓	AR-12B 7 "	1										
56138	6/6/86	1547		✓	AR-13A 3 "											
56139	6/6/86	1548		✓	AR-13B 7 "											
56140	6/6/86	1550		✓	AR-14A 3 "											
56141	6/6/86	1552		✓	AR-14B 7 "											

RELINQUISHED BY (SIGNATURE): <i>Stephen O'Neil</i>	DATE/TIME: 6/9/86 1700	RECEIVED BY (SIGNATURE): <i>Federal Express Air Bill #02745</i>	RELINQUISHED BY (SIGNATURE): <i>Federal Express Air Bill #02745</i>	DATE/TIME: 6/10/86 1100	RECEIVED BY (SIGNATURE): <i>Helen H. Watson</i>
RELINQUISHED BY (SIGNATURE): <i>Helen H. Watson</i>	DATE/TIME: 6/10/86 1300	RECEIVED BY (SIGNATURE):	RELINQUISHED BY (SIGNATURE):	DATE/TIME:	RECEIVED BY (SIGNATURE):
RELINQUISHED BY (SIGNATURE):	DATE/TIME:	RECEIVED FOR LABORATORY BY (SIGNATURE): <i>Robt E. Wagner</i>	DATE/TIME: 6/10/86 1300	REMARKS:	

Distribution: Original accompanies shipment; copy to coordinator field files.

### CHAIN OF CUSTODY RECORD

[illegible]

GHR Analytical Inc.  
26 Main St., Lakeville, MA

CHAIN OF CUSTODY RECORD

Page 1 of 2

PROJECT NO.: 29-297		WORK PLAN NO.:		SITE NAME: Acushnet River Estuary		NO. OF CON- TAINERS											REMARKS
SAMPLERS (SIGNATURE): <i>Stephen O'Neil</i>				EAST BANK													
STATION NO.	DATE	TIME	COMP.	GRAB	STATION LOCATION												
56242	6/10/86	1500		✓	AR-18A 3 inch depth	1											
56243	6/10/86	1503		✓	AR-18B 7 " "	1											
56244	6/10/86	1510		✓	AR-19A 3 " "	1											
56245	6/10/86	1513		✓	AR-19B 7 " "	1											
56246	6/10/86	1520		✓	AR-20A 3 " "	1											
56247	6/10/86	1525		✓	AR-20B 7 " "	1											
56248	6/10/86	1530		✓	AR-21A 3 " "	1											
56249	6/10/86	1535		✓	AR-21B 7 " "	1											
56250	6/10/86	1615		✓	AR-22A 3 " "	1											
56251	6/10/86	1620		✓	AR-22B 7 " "	1											
56252	6/10/86	1625		✓	AR-23A 3 " "	1											
56253	6/10/86	1630		✓	AR-23B 7 " "	1											
56254	6/10/86	1632		✓	AR-25A 3 " "	1											
56255	6/10/86	1635		✓	AR-25B 7 " "	1											
RELINQUISHED BY (SIGNATURE): <i>Stephen O'Neil</i>		DATE/TIME: 6/11/86 1815		RECEIVED BY (SIGNATURE): Federal Express Air Bill # 731653873		RELINQUISHED BY (SIGNATURE): Federal Express Air Bill # 731653893		DATE/TIME: 6/12/86 1300		RECEIVED BY (SIGNATURE): <i>Helen H. Wooten</i>							
RELINQUISHED BY (SIGNATURE): <i>Helen H. Wooten</i>		DATE/TIME: 6/12/86 1500		RECEIVED BY (SIGNATURE):		RELINQUISHED BY (SIGNATURE):		DATE/TIME:		RECEIVED BY (SIGNATURE):							
RELINQUISHED BY (SIGNATURE):		DATE/TIME:		RECEIVED FOR LABORATORY BY (SIGNATURE): <i>Robert E. Wagon</i>		DATE/TIME: 6/12/86 1400		REMARKS:									

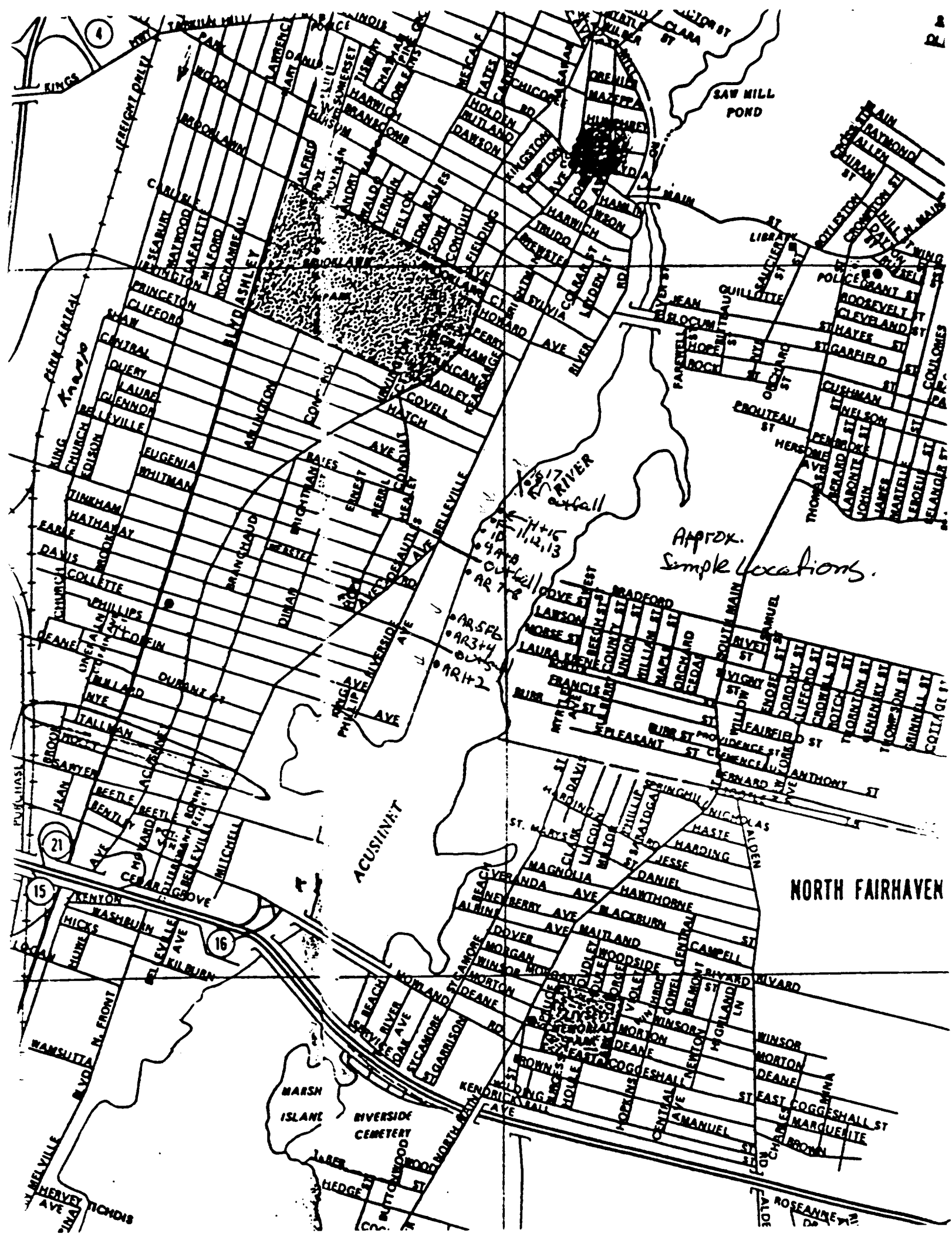
### CHAIN OF CUSTODY RECORD

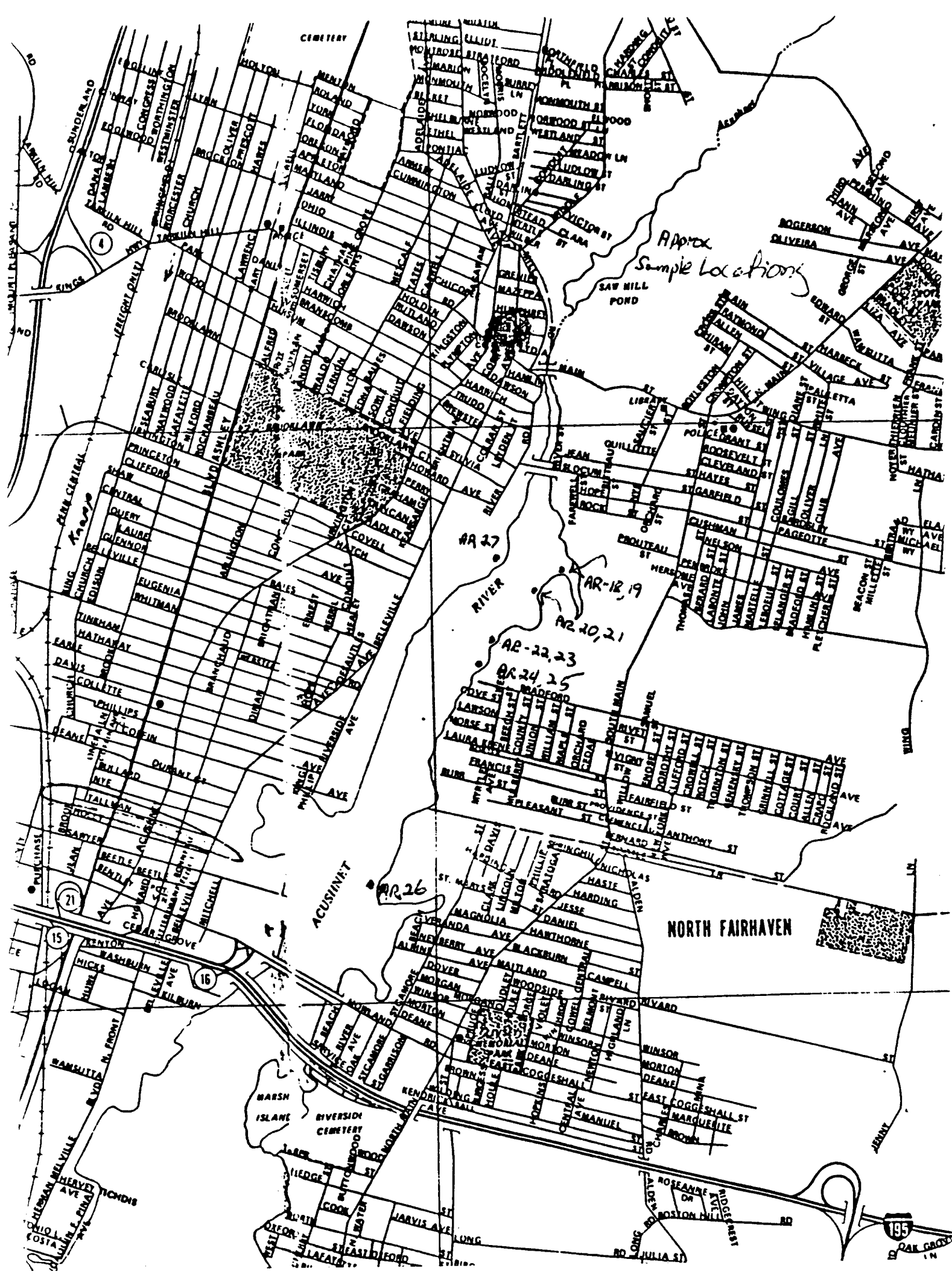
Page 282

[illegible]

**Distribution:** Original accompanies shipment; copy to coordinator field files







Approx  
Sample Locations

AR 27  
RIVER

AR 18, 19  
AR 20, 21

AR 22, 23  
AR 24, 25

AR 26

NORTH FAIRHAVEN

Samples Received from GHR, June 10, 1986  
(Collected by "S.O.") GC Analyzed July 1-2, 1986

GHR Analyst  
No

Time  
Collected:

Submitted to RE Wagner for analysis,  
6/10/86 \*

GR-

Sample  
Location

6/6/86

Appearance, odor of sample

56114	1	AR-1A	1335		Coarse sand, shells - grayish
5	2	1B	1339		" " "
6	3	2A	1345	X	gravel, sand, mud - odor of fuel oil - b/n
7	4	2B	1349	X	" " "
8	5	3A	1356		gravel, sand, <u>mud</u> - black
9	6	3B	1400		" " "
20	7	4A	1405		gravel sand, mud, black
1	8	4B	1407		" " mud? grayish
2	9	5A	1410	X	Fine black sand - slightly coherent
3	10	5B	1418	X	Fine grayish-black sand - slightly coherent
56124	11	6A	1416		Black <sup>fine</sup> mud + cylindrical objects
5	12	6B	1416		Grayish-black organic mud + 1 cylindrical obj.
6	13	7A	1448		Coarse brown sand, shells
7	14	7B	1450		" " "
8	15	8A	1453		Brown gravel, sand, shells, sediment
9	16	8B	1455		" " "
30	17	9A	1500	XX	Gravel + organic mud
1	18	9B	1503	X	" " "
2	19	10A	1525		Coarse brown sand, gravel
3	20	10B	1526		" " "
56134	21	11A	1528		Brown gravel + fine sand
5	22	11B	1532		" " "
6	23	12A	1542	X	Dark gray - coarse sand, gravel, + mud?
7	24	12B	1545	X	" " "
8	25	13A	1547		" " "
9	26	13B	1548		" " "
40	27	14A	1550	XX	Large <sup>coherent</sup> grayish-brown organic mud a fine
1	28	14B	1552	X	" " "
2	29	15A	1555		" " "
3	30	15B	1557		" " "
56144	31	16A	1605		" " black
5	32	16B	1610		" " grayish
6	33	17A	1615	X	" " black
56147	34	17B	1620	X	" " black

H<sub>2</sub>S odor

Samples Rec'd for GHR, June 13, 1986

GC Analyzed July 14-16, 1986

6-10-86

GR -	Sample Locals	Time Collected		
56242	001	HR-15A	1500	X grey brown sand. Slightly <del>fibrous</del> <sup>fibrous</sup>
3	2	15B	1503	X " "
4	3	15A		X black mud. H <sub>2</sub> S odor.
5	4	15B		X " " sl. H <sub>2</sub> S <del>odor</del> -
6	5	20A		<del>X</del> sand + organic fiber
7	6	20B		" " + pebbles
8	7	21A		X sand + mud + rubble
9	8	21B		X " (") "
56250	9	22A		X sand + fiber
1	10	22B		X " " + pebbles
2	11	23A		mainly sand coarse
3	12	23B		" " "
4	13	25A		" " "
5	14	25B		" " "
6	15	24A		X fine brownish sand
7	16	24B		X " " "
8	17	17C		<del>mainly sand</del> pure sand
9	18	27		pure sand
60	19	26A	1725	X marked
61	020	26B	1732	X marked

\* Basis for sample selection on 6/10/86:

- Total number of sites to be included in investigation only 12 (6 on east side of estuary, 6 on west) rather than the 26 for which samples collected, despite my request for only 12 pairs of samples.
- In selecting sites for study, rejected a few where sample all stones, gravel, coarse sand -- anticipated a low PCB content.
- Otherwise, selected samples so as to give relatively even spacing of sites, and variety of sediment types.

GHR ANALYTICAL, INC.  
26 MAIN STREET  
LAKEVILLE, MA 02347  
(617) 947-5077

*Agg VAX*  
*995-5136*

RESULTS OF SEDIMENT ANALYSIS  
Acushnet River Estuary  
Date Collected: June 6, 1986

Client: General Electric  
Project: Oil & Grease Analyses

Job No.: 29-272  
Date: June 17, 1986

<u>Sample Location</u>	<u>Depth</u>	<u>GHR Lab ID</u>	<u>Oil &amp; Grease</u> <u>mg/kg (dry weight basis)</u>
AR-1A	3"	56114	1,040
AR-1B	7"	56115	780
AR-2A	3"	56116	1,570
AR-2B	7"	56117	2,050
AR-3A	3"	56118	1,700
AR-3B	7"	56119	2,430
AR-4A	3"	56120	2,630
AR-4B	7"	56121	980
AR-5A	3"	56122	12,800
AR-5B	7"	56123	34,500
AR-6A	3"	56124	78,000
AR-6B	7"	56125	172,000
AR-7A	3"	56126	19,300
AR-7B	7"	56127	6,100
AR-8A	3"	56128	3,590
AR-8B	7"	56129	1,220
AR-9A	3"	56130	26,700
AR-9B	7"	56131	22,900
AR-10A	3"	56132	1,260
AR-10B	7"	56133	421
AR-11A	3"	56134	926
AR-11B	7"	56135	261

*Lucan*

GHR ANALYTICAL, INC.  
 26 MAIN STREET  
 LAKEVILLE, MA 02347  
 (617)947-5077

# RESULTS OF SEDIMENT ANALYSIS

Acushnet River Estuary  
 Date Collected: June 6, 1986

Client: General Electric  
 Project: Oil & Grease Analyses

Job No: 29-272  
 Date: June 17, 1986

<u>Sample Location</u>	<u>Depth</u>	<u>GHR Lab ID</u>	<u>Oil &amp; Grease</u> <u>mg/kg (dry weight basis)</u>
AR-12A	3"	56136	8,730
AR-12B	7"	56137	6,070
AR-13A	3"	56138	10,900
AR-13B	7"	56139	4,840
AR-14A	3"	56140	3,840
AR-14B	7"	56141	3,390
AR-15A	3"	56142	2,680
AR-15B	7"	56143	2,990
AR-16A	3"	56144	16,300
AR-16B	7"	56145	21,600
AR-17A	3"	56146	46,300
AR-17B	7"	56147	40,300

GHR ANALYTICAL, INC.  
 26 MAIN STREET  
 LAKEVILLE, MA 02347  
 (617) 947-5077

# RESULTS OF SEDIMENT ANALYSIS

Acushnet River Estuary  
 Date Collected: June 10, 1986

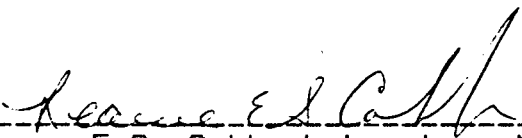
Client: General Electric  
 Project: Oil & Grease Analyses

Job No.: 29-297  
 Date: June 17, 1986

Sample Location	Depth	GHR Lab ID:	Oil & Grease mg/kg (dry weight basis)
AR-18A	3"	56242	20,700
AR-18B	7"	56243	7,040
AR-19A	3"	56244	20,000
AR-19B	7"	56245	28,400
AR-20A	3"	56246	5,290
AR-20B	7"	56247	306
AR-21A	3"	56248	11,100
AR-21B	7"	56249	1,440
AR-22A	3"	56250	5,390
AR-22B	7"	56251	8,110
AR-23A	3"	56252	1,700
AR-23B	7"	56253	794
AR-24A	3"	56256	<150
AR-24B	7"	56257	<150
AR-25A	3"	56254	968
AR-25B	7"	56255	484
AR-26A	3"	56260	<440
AR-26B	7"	56261	<370

GHR ANALYTICAL INC.  
26 MAIN STREET  
LAKEVILLE, MA 02347  
(617) 947-5077

The information contained in this report is to the best of my  
knowledge, accurate and complete.

  
-----  
Leanne E.S. Cobb, Laboratory Manager  
GHR Analytical Inc.



**GE Corporate Research and Development Center**

***Material Characterization and Engineering Support Operation***

***Separations and Molecular Weights Lab***

**PCB MANUAL**

## Table of Contents

Part 1 - Organization Chart

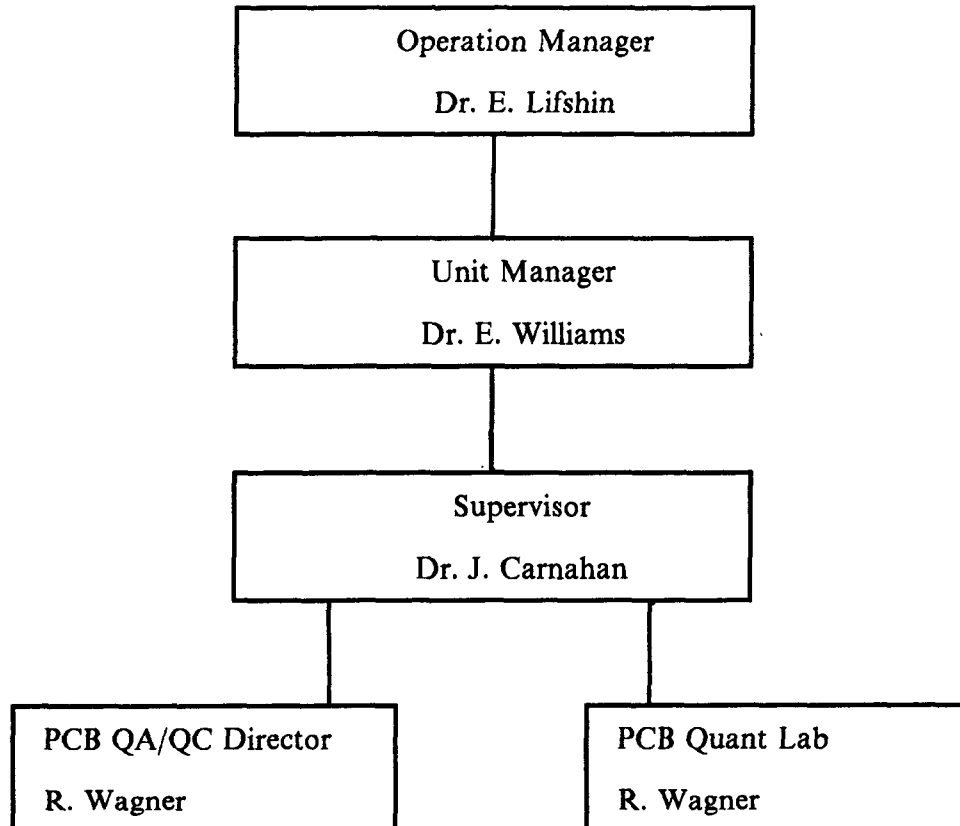
Part 2 - QA/QC Protocol

Part 3- References

Part 4 - PCB Protocol Manual

## ***Part 1 - Organization Chart***

*Organization Chart*



## ***Part 2 - QA/QC Protocol***

## **Quality Assurance and Quality Control**

### ***Sample Chain Of Custody***

Samples entering the Lab are directed to the chemist who is in charge of the particular analysis requested. All samples are recorded into a sample notebook and assigned a sample ID number. A sample information sheet corresponding to the sample notebook number is filled in with all the necessary sample information. A peel off label with the sample ID number is attached to the vial containing the sample and the sample is then stored under appropriate conditions.

### ***Calibration***

Before every group of PCB analyses a Standard Aroclor is analyzed on the GC to check the calibration accuracy. If we find the Aroclor standard varies more than  $\pm 10\%$  from true value, the instrument is calibrated and a standard is once again checked before samples are analyzed.

### ***Aroclor Standard Reference***

Aroclor standards were obtained from the CR&D stockroom, supplied by Monsanto Co. for GE's research programs. These bulk neat standards have been checked against NBS certified Aroclor in Oil standards as well as the Water Pollution QC samples supplied by EMSL, Quality Assurance Branch, USEPA, Cinn., OH. Our in-house standards agree very well with the two certified check samples.

### ***Sample Precision and Accuracy***

Accuracy of the instrumentation is tested by running standards to check on calibration quality. Testing extraction and clean up procedures were done when they were being developed to insure no sample loss at each step. If any changes occur in sampling methodology, it is checked with processing standards to insure sample integrity is being maintained. Precision of the analytical instrumentation is tested by occasionally running samples twice. Duplicate agreement must be maintained to  $\pm 10\%$ . Testing procedures were initially examined using standardized materials and run separately to insure reproducibility and therefore good precision.

### ***Blanks***

Solvent wash vials are added at the end of a group of samples. This allows us to clean the sampling system and also to check for baseline deviations or matrix effects and spurious peaks.

### ***Data Reduction and Reporting***

Refer to the PCB protocol manual for examples of GC data reporting. Data is collected by digitizing an analog detector signal and electronically integrating the area under a peak. Most instrument companies have available integrators that match their GC instrumentation and all GC integration is done automatically. Final result calculations can be programmed into the integrator and directly report sample amounts in the appropriate units (ug/g, ug/ml, ppm, etc.)

### ***Instrument Conditions***

See PCB Protocol Manual

### ***Sample Preparation***

See PCB Protocol Manual

### ***Instrument Maintenance***

The GC is maintained usually by the chemist who is utilizing the instrument, since he is most familiar with its status. Gas tanks are inspected and changed as needed. Injection port septa are changed after 50-60 injections. Noise level of the GC detector is monitored and the detector replaced once it become excessive. GC columns are replaced as needed, either if they become badly contaminated or have reached their lifetime and no longer perform the separation properly.

### ***Part 3 - References***



## ***References***

The following references have been used to develop the PCB methodology used at GE CR&D.

"Handbook of Quality Assurance for the Analytical Chemistry Laboratory", J Dux, Van Nostrad Reinhold publisher, 1986

"The Determination of PCB in Transformer Fluid and Waste Oils", TA Bellar & JJ Litchenberg, USEPA, 1981

"Quantitative PCB Standards for Electron Capture Gas Chromatography", RG Webb & AC McCall, Journal of Chromatographic Science, Vol 11, pp 366-373, 1973

"Recommended Analytical Requirements of PCB Data Generated On Site During Non-Thermal PCB Destruction Tests", USEPA, March 19, 1986

"The Federal Register, Title 40 CFR, Intermin Guidelines for Establishing Testing Procedures", USEPA, 1979

"Analytical Chemistry of PCBs", MD Erickson, Butterworth Publishers, 1986

"The Chemistry of PCB's", O Hutzinger, S Safe, & V Zitko, CRC Press, 1974

## ***Part 4 - PCB Protocol Manual***

# PCB PROTOCOL

## INTRODUCTION

This protocol details the analysis of polychlorinated biphenyls (PCB's). The analytical procedure can be divided into three sections:

- I. Sample collection, preparation, and extraction: this section describes how to collect samples, preliminary sample preparation, and extraction of PCB's from the following sample matrices- soil and sediments, water, fish and other biological samples, oil, and air.
- II. Sample cleanup: this section describes the steps necessary to remove any materials co-extracted with the PCB's that may interfere with the subsequent analysis.
- III. Analysis: this section describes both the qualitative and quantitative analysis of PCB's by either packed or capillary column gas chromatography.

In addition, there are general guidelines which are followed for all sample types. These involve the types of materials which may contact the samples, how to clean glassware, and the quality of chemicals and solvents which must be used in the procedure.

## PCB PROTOCOL

### 1.0 GENERAL PROCEDURES

#### 1.1 Glassware

To prevent interference in the analysis of trace substances, all glassware must be washed thoroughly prior to use. Specialty glassware is washed with soap and water and thoroughly rinsed with water. Next, it is rinsed with acetone, followed by hexane. Stockroom glassware is visually inspected for cleanliness. As an additional precaution, each piece of clean glassware is rinsed with hexane immediately prior to use.

#### 1.2 Chemicals

All chemicals and solvents must be ACS reagent grade or better.

#### 1.3 Other materials

No equipment containing plastic may be used. Plastic materials (such as Tygon tubing) give off phthalate esters, which interfere with PCB analysis and are difficult to remove. Only materials made from glass, teflon, or stainless steel may contact the sample during the procedure. All utensils must be pre-rinsed with hexane. All containers must be glass and have a teflon or foil-lined lid. All tubing used during such steps as solvent evaporation or vacuum drying must be either teflon or stainless steel.

## PCB PROTOCOL

### 2.0 SAMPLE COLLECTION, PREPARATION, AND EXTRACTION

#### 2.1 Soil and Sediments

##### 2.1.1 Sample collection

Soil and sediment should be collected in a wide-mouthed one quart screw-capped glass jar. The jar should be filled nearly to the top, using a pre-rinsed stainless steel utensil. If the sample is sediment, it should be "topped off" with sample water. The sample should be extracted as soon as possible; until extraction it should be stored at 4 degrees C.

##### 2.1.2 Sample preparation

The whole sample(if practical) or a representative portion is spread out in a pyrex dish and allowed to air-dry for 24 hours in a hood. The sample is then sieved through a wire mesh screen to remove twigs and stones, and thoroughly mixed. An aliquot is placed in a small tared metal pan and dried overnight at 105 degrees C in a vacuum dessicator oven for dry weight determination. A separate aliquot(commonly 20-30g) is taken for extraction.

##### 2.1.3 Extraction

Soil and sediment samples are extracted in a soxhlet apparatus. The standard-sized round-bottomed flask used is 250 ml and the standard thimble is a Whatman cellulose thimble with the dimensions 33 mm I.D. by 94 mm external length. The complete apparatus,including thimble and glass wool plug, is pre-extracted with hexane for several cycles(approximately 1 hr), allowed

## PCB PROTOCOL

to cool and the thimble allowed to air-dry. The sample is weighed into the tared thimble and the glass wool plug is inserted on top of the sample. A pre-extracted boiling stone is added to the boiling flask. The soil is then extracted overnight with 175 ml of a 1:1 mixture of hexane:acetone, and the apparatus is allowed to cool. All solvent is drained from the soxhlet into the round-bottomed flask.

### 2.2 Aqueous samples

#### 2.2.1 Sample collection

Water samples are collected and stored in a manner similar to that for the collection of soil and sediment, as explained in Section 2.1.1.

#### 2.2.2 Sample preparation

The aqueous sample is thoroughly shaken to evenly suspend any solids. If it is desirable to remove solids, the water is filtered through pre-extracted filter paper. Since aqueous solubility of PCB's is extremely low, a minimum water sample of 100 ml is desirable.

#### 2.2.3 Extraction

Pour a known volume of aqueous sample into an appropriately sized glass bottle. Rinse the graduated cylinder used to measure the sample volume with 20 ml of a 15% methylene chloride in hexane solution(per 100 ml of sample) and add it to the glass bottle containing the sample. Cap the bottle, manually shake it and vent the vapor pressure as necessary, and place it on a

## PCB PROTOCOL

mechanical shaker for 20 minutes.

Allow the layers to separate. If an emulsion forms, add some sodium chloride and mix by inverting the bottle 2-3 times. If this does not separate the layers, the sample may be sonicated for several minutes. Withdraw the upper organic layer with a 10 ml pipet and transfer it to a 100 ml glass bottle. Re-extract the aqueous layer 2 more times as described; combine the organic layers.

### 2.3 Biological samples

#### 2.3.1 Sample collection

The fish or other samples are collected, individually wrapped in hexane-rinsed aluminum foil, and frozen until subsections can be taken.

#### 2.3.2 Sample preparation

Prior to subsectioning each sample is thawed and weighed. The sample is subsectioned as desired and a minimum of 20 grams wet weight is used for the analysis(if possible). The sample is scissor-minced as finely as possible and suspended in approximately 50 ml of water in a 150 ml beaker. The sample is homogenized with a Brinkman Instruments Polytron. The Polytron probe is pre-rinsed by submerging it in hexane and turning the Polytron on. Homogenize at a low to medium setting(be careful not to splash) until the sample is a uniform consistency. The probe must be frequently cleared of connective tissue buildup during this process for efficient homogenization. To accomplish

## PCB PROTOCOL

this, turn off the instrument and use forceps to remove lumps of connective tissue from the probe tip. These may be minced and returned to the sample beaker.

The homogenate is next ground with anhydrous magnesium sulfate to further disintegrate the sample and to combine with the water that is present. This is accomplished in the following manner: transfer the homogenate to a glass mortar, using small quantities of water to rinse the beaker if necessary. Weigh magnesium sulfate in the ratio of 3.2 grams of magnesium sulfate per gram of wet tissue weight. Add the magnesium sulfate, in small portions, to the homogenate, using a glass pestle to mix it in and grind up any lumps. Transfer the resulting wet granular mixture to a glass petri dish and spread it out to dry. As the mixture dries, transfer it back into the mortar, small portions at a time, and grind thoroughly until a fine, free-flowing powder is obtained.

### 2.3.3 Extraction

Pre-extract the soxhlet apparatus as described in Section 2.1.3, using a thimble of dimensions 43 mm I.D. by 123 mm external length and a 500 ml round bottomed flask. Soxhlet-extract the sample as described in Section 2.1.3, using 350 ml of 1:1 hexane:acetone.

### 2.4 Oil

A Florisil Sep-Pak is pre-eluted with 10 ml hexane and dried by pulling a vacuum through it. The Sep-Pak is placed in a 4 dram vial and tared. The oil is



## PCB PROTOCOL

thoroughly mixed and 200 mg is weighed directly into the Sep-Pak using a syringe. The Sep-Pak is then attached to a 10 ml glass syringe and the PCB's are eluted with hexane directly into a 10 ml volumetric flask. At this point the oil sample should be ready for GC analysis. If the extract is not colorless, a sulfuric acid wash may be necessary (see Section 3.4).

### 2.5 Air

#### 2.5.1 Sample collection

Air samples are collected using a calibrated air sampling pump(Bendix Environmental and Process Instruments Division) equipped with a Florisil trapping tube(SKC Inc.,Pa.,cat # 226-39). The pump is placed near a contamination source , turned on, and allowed to run for 24 hours(note actual collection time). The packing in the trapping tube is divided into 2 sections. The glass tube is broken and these 2 sections are poured into 2 dram vials and extracted separately in order to determine whether there is PCB breakthrough, which indicates sample overload.

#### 2.5.2 Extraction

The Florisil fractions are shake-extracted 3 times for 20 minutes each time with small aliquots(approximately 1-2 ml) of hexane. The Florisil is allowed to settle after each extraction and the hexane is transferred to a 2 dram vial with a pasteur pipet. The combined hexane extracts are reduced in volume using a Pierce Reacti-therm Module(as described in Section 3.2) to 1.0

## PCB PROTOCOL

ml for analysis.

## PCB PROTOCOL

### 3.0 SAMPLE CLEANUP

#### 3.1 Sodium sulfate drying

Add a sufficient quantity of anhydrous sodium sulfate to the crude extract such that the crystals are free-flowing. Pour a 10 cm column of sodium sulfate in a glass chromatography column, 2.5 cm I.D., equipped with a teflon stopcock. Wash the sodium sulfate with at least one bed volume of hexane. Pour the crude extract through the column (a funnel helps to load the column) and collect the eluate in an appropriately sized glass bottle. Rinse the sample flask, the funnel, the column walls and the sodium sulfate 3 times with small volumes of hexane and add the washings to the extract.

#### 3.2 Reduction of sample volume

The sample volume is reduced to approximately 5 ml on a steam bath, using a Kuderna-danish equipped with a 3-ball Snyder column and a 10 ml concentrator tube. A pre-extracted boiling stone is added to prevent bumping. The extract is placed in the assembled apparatus, the sample bottle is rinsed 3 times with hexane, and the washings added to the apparatus. After the inner walls of the Kuderna-danish are rinsed down, the Snyder column is put in place, and a small volume of hexane is added at the top. The apparatus is placed in a steam bath and the solvent is evaporated. Take care to control the boiling intensity; solvent should not splash up high on the inner walls of the apparatus.

## PCB PROTOCOL

If a large volume must be reduced, add the extract in aliquots of approximately 200 ml, cooling before each addition, and adding a fresh boiling stone.

When the total extract volume is approximately 5 ml, allow the apparatus to cool. The extract is quantitatively transferred to a 4 dram vial to complete the solvent evaporation. This is done as follows: remove the Snyder column from the top of the apparatus. Carefully dry the joint connecting the concentrator tube and the Kuderna-danish so that condensation does not drip into the extract. Separate the pieces and transfer the extract to the vial using a pasteur pipet. Reconnect the pieces and wash the inside walls of the Kuderna-danish with a small volume of hexane (approximately 2-3 ml). Add the washings to the extract and repeat the rinsing process 2 more times. The remainder of the solvent is evaporated under a stream of Femtogas nitrogen, using low heat (low setting 3.5 on Pierce Reacti-therm Module). Twenty-five microliters of hexadecane is added to prevent evaporative loss of lower chlorinated PCB isomers. When the sample reaches dryness, remove it from the heat source and reconstitute it in approximately 2-3 ml hexane. If there is a large amount of viscous or dark-colored residue a sulfuric acid wash may be necessary at this point (see Section 3.4). If not, Florisil chromatography is the next step.

### 3.3 Florisil chromatography

This procedure should result in a clear, colorless extract. The extract is passed through a Florisil Sep-Pak attached to a glass syringe and collected in a 10 ml volumetric flask. Pre-elution of the Sep-Pak with 10 ml hexane is advisable. The 4 dram vial, then the inner walls of the syringe are rinsed 3 times with hexane and the washings are passed through the Sep-Pak. The sample is adjusted to final volume with hexane and transferred to a screw-capped vial for storage. At this point the sample is ready for GC analysis. If the chromatogram shows the presence of sulfur or other extraneous peaks, a copper treatment for sulfur removal or a concentrated sulfuric acid wash for hydrocarbon removal may be necessary.

### 3.4 Sulfuric acid wash

The sulfuric acid wash destroys hydrocarbons and colored biogenic compounds which appear as early-eluting peaks on the chromatogram. (If the presence of surfactants or alkali are suspected, water wash the extract before the sulfuric acid wash. The water wash procedure is identical to the acid wash. Do not dry the resulting hexane solution with sodium sulfate before the acid wash, and reduce the volume to approximately 5 ml.) Add an equal volume of concentrated sulfuric acid to the hexane in a 4 dram vial. The contents are mixed by inverting the vial several times (vigorous shaking can cause emulsions)

## PCB PROTOCOL

and the layers are allowed to separate. If an emulsion forms, sonicate the vial for several minutes. Do not add sodium chloride!

Remove the top hexane layer and wash the sulfuric acid layer two times with approximately 2 ml hexane. Combine all hexane solutions. Add a small amount of sodium sulfate to dry the extract, reduce the volume using the Reacti-therm module to 2-3 ml and pass the extract through a Florisil Sep-Pak as before.

### (3.5 Copper treatment)\*

This treatment removes sulfur compounds which may be found, especially in soil and sediment. The presence of sulfur is indicated as a large, early-eluting lump in the baseline or as a large, offscale peak. The hexane extract is stirred with 0.5 grams of activated copper for 30 minutes. (copper activation: wash with 200 ml of 0.01M nitric acid, followed by successive 200 ml rinses of distilled water, acetone, and hexane. Air-dry the powder, which should be bright red-orange and store in a screw-capped vial. Powder should be used within 48 hr) The copper is allowed to settle and the hexane is removed. The vial and copper are rinsed 3 times with small amounts of hexane; the hexane solutions are combined. The solution is reduced in volume on the Reacti-therm and passed through a Florisil Sep-Pak.

\* Now use mercury instead, as in EPA Method 608

## PCB PROTOCOL

### 4.0 ANALYSIS

PCB's can be analyzed by either packed or capillary column GC, depending on the type of analysis required. Packed column analysis is routinely used to determine total PCB content for single Aroclors and mixtures. The weight percent of each peak in the chromatogram of single Aroclors has been determined by Webb and McCall (J. Chrom. Sci., 11, 366 (1973)). In addition, a program has been developed which calculates the total PCB's present, from monochloro- to octachlorobiphenyl, using a mixture of Aroclors 1242 and 1260, which spans the whole range of isomers present in Aroclors 1242, 1248, 1254, and 1260. For any mixture of 1242, 1254, and 1260 this program can also calculate the approximate percent composition, based on a peak ratio technique.

However, the isomer resolution afforded by packed column analysis is not sufficient to perform single isomer quantitation, the Aroclor composition of complex mixtures, or the relative percent contribution of each Aroclor when those percents are very different. Capillary GC is the preferred analysis when this type of information is required.

#### 4.1 Packed column analysis

The instrument used for packed column analysis is a Hewlett Packard 5880 equipped with Autosampler model 7672A. The GC conditions are as follows:

# PCB PROTOCOL

Column=mixed silica, 1.5% SP2250 and 1.95% SP2401 on  
Supelcoport, 6 ft. by 0.25 in. O.D. glass

Oven temperature profile

equilibration time=1.0 min.

initial value=150 C

initial time=0.0 min.

level 1

program rate=2.0 C/min.

final value=210 C

final time=30.0 min

post value=150 C

nickel ECD detector temperature=300 C, signal B

injector temperature=300 C

injection volume=1 microliter

carrier gas

type=5% methane in argon

flow=60 ml/min.

chart speed=0.5 cm/min.

offset=10

attenuation=8

threshold=2

peak width=0.15

The sample is visually inspected for Aroclor type and the presence of interferences. Samples are then quantitated by comparing the chromatogram to that of a known Aroclor, using a multi-level external standard calibration based on peak height and covering the range of 0.1 to 10.0 PPM. Sample tracings of 10 PPM



## PCB PROTOCOL

standards of Aroclors 1242, 1254, and 1260 are shown in Figures 1, 2, and 3. Figure 4 shows a sample output of the type of information given in the program which calculates the total PCB content and relative percent composition.

### 4.2 Capillary column analysis

The instrument used for capillary column analysis is a Varian 4600 equipped with Autosampler model 8000 and a Vista 401 data system. The GC conditions are as follows:

column=DB-1 fused silica(J and W), 30 m.

oven temperature profile

initial value=40 C

initial time=2.0 min.

level 1

program rate=10.0 C/min.

final value=80 C

final time=0.0 min.

level 2

program rate=6.0 C/min.

final value=225 C

final time=10.0 min.

nickel ECD detector temperature=300 C, signal A

range=10

make-up gas=nitrogen

injector temperature=300 C

injection volume=2 microliters

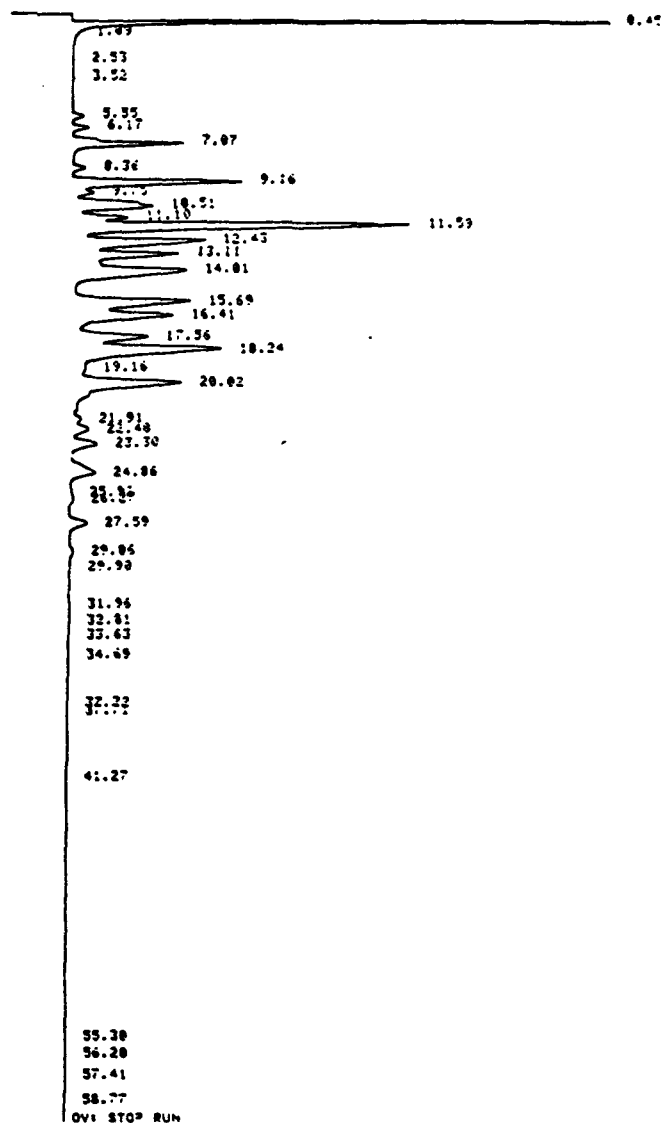
splitless injection

## PCB PROTOCOL

vent off at injection  
vent on at 0.4 min. post injection  
carrier gas type=helium  
flow=30cm/sec.  
chart speed  
0.0-20.0 min=0.1 cm/min.  
20.0-end=0.5 cm/min.  
offset=10  
attenuation=16

Samples are quantitated by comparison to a known Aroclor, using an external standard calibration based on peak height. Figures 5, 6, and 7 show capillary GC tracings of 2 PPM standards of Aroclors 1242, 1254, and 1260.

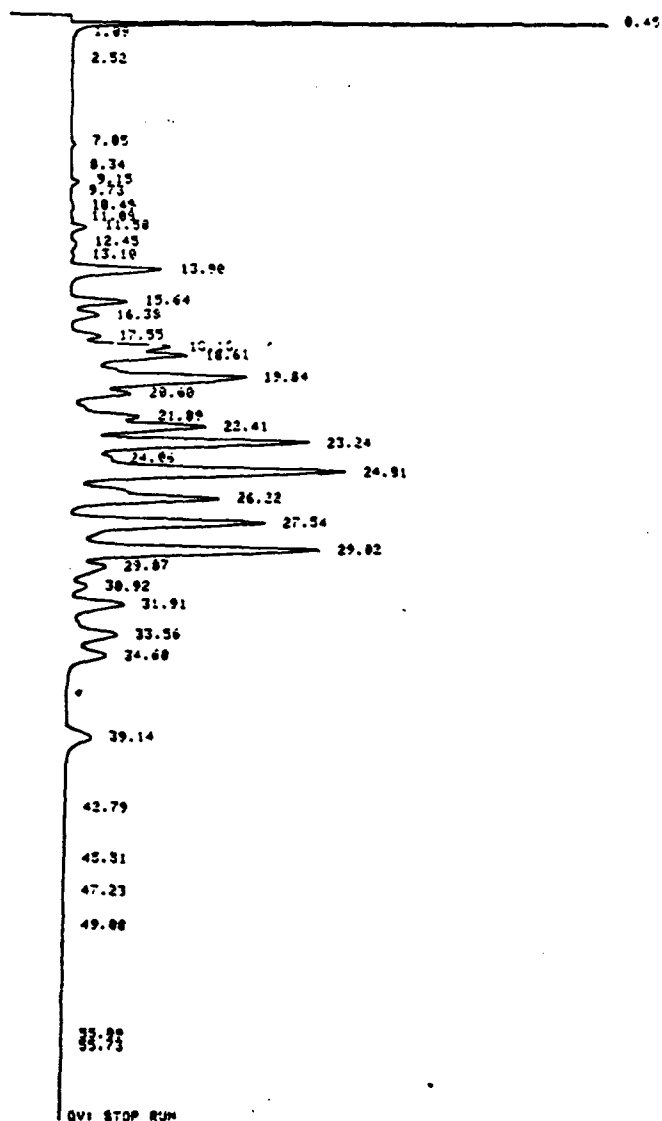
Fig 1



END 3 5888A SAMPLER INJECTION 0 20:07 DEC 20, 1982  
 SAMPLE 0 1 ID CODE 1  
 3 1242/10.3  
 1260 ON CLEARED EC  
 ESTD COMPENSATED ANALYSIS

RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00			BASELINE 0 START RUN = 163.52				
0.00			THRESHOLD 0 START RUN = 2				
0.00			PEAK WIDTH 0 START RUN = 0.15				
3.52	3.53	11.50	BB	0.127	1	0.161	1
5.35	5.36	86.70	BB	0.218	2	0.449	2
6.17	6.18	123.20	VV	0.224	3	0.199	2
7.07	7.08	785.67	VV	0.277	4	1.310	2
9.16	9.18	1199.05	VV	0.277	5	1.494	2, 3
10.51	10.53	578.84	VV	0.312	6	0.832	3
11.39	11.41	2351.22	VV	0.312	7	1.484	3
12.43	12.44	929.16	VV	0.312	8	1.449	3
14.01	14.02	810.72	VV	0.312	9	1.165	4
15.69	15.71	836.28	VV	0.312	10	0.891	3, 4
16.41	16.42	718.77	VV	0.312	11	0.749	4
18.24	18.26	1056.94	VV	0.312	12	1.297	4, 5
20.02	20.04	781.46	VV	0.312	13	0.817	4, 5
22.48	22.49	133.13	VV	0.312	14	0.171	5
23.30	23.32	198.67	VV	0.453	15	0.272	5
24.86	24.87	184.18	VV	0.453	16	0.189	5, 6
27.59	27.60	129.23	PS	0.400	17	0.119	

MULTIPLIER = 1



E-3 58804 SAMPLE INJECTION @ 00:34 DEC 21, 1982

SAMPLE # : 19 CODE :

7 1254/10.4

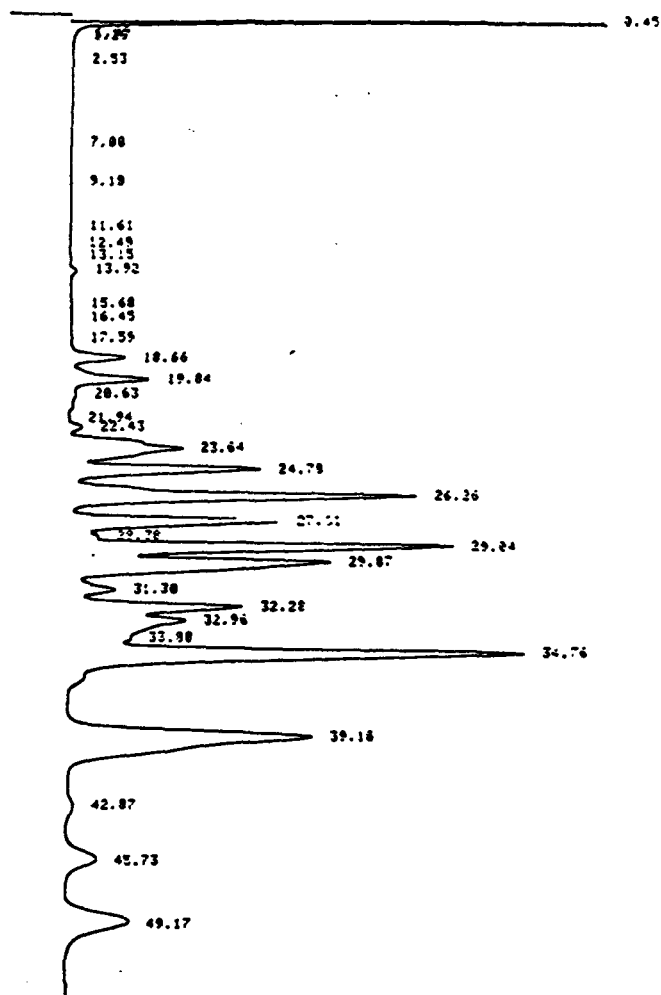
1260 ON CLEANED EC

ESTS COMPENSATED ANALYSIS

RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00							
0.30							
0.90							
18.61	18.66	829.38	VV	-----	1	0.458	3
19.84	19.84	1236.43	VV	-----	2	1.195	3
23.24	23.64	1681.20	VV	-----	3	1.719	3.6
24.91	24.70	1945.27	VV	0.511	4	2.842	3.6
26.22	26.26	1052.91	VV	-----	5	0.667	6
27.54	27.61	1377.48	VV	-----	6	0.528	6.7
29.82	29.84	1764.35	VV	0.479	7	0.924	6
29.87	29.87	269.61	VV	-----	8	0.129	6.7
31.91	32.20	480.70	VV	-----	9	0.232	6.7
33.56	32.96	351.48	VV	-----	10	0.156	7
34.68	34.76	279.60	VV	-----	11	9.851E-02	7
39.14	39.18	102.10	BV	0.747	12	8.374E-02	7.0
45.31	45.73	3.97	BP	-----	13	1.201E-03	8
49.08	49.17	10.22	VB	-----	14	3.674E-03	8

MULTIPLIER = 1

Fig 3



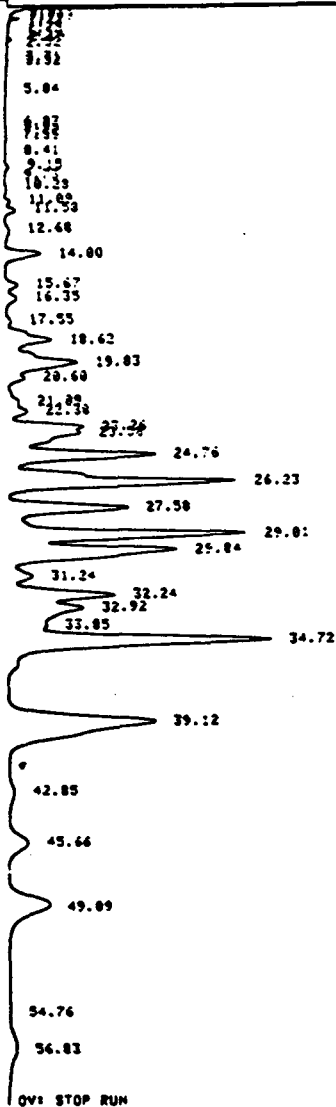
EXP 3 5380A SAMPLER INJECTION 0 16:22 DEC 20, 1982  
 SAMPLE 0 : ID CODE :  
 3 1260/11.6  
 1260 ON CLEARED EC  
 ESTD COMPENSATED ANALYSIS

RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00							
0.00							
0.00							
BASELINE 0 START RUN = 156.83							
THRESHOLD 0 START RUN = 2							
PEAK WIDTH 0 START RUN = 0.15							
10.66	10.72	394.11	VV	0.421	1	0.332	5
19.84	19.90	561.98	VV	0.421	2	0.561	5
23.64	23.71	885.54	VV	0.421	3	0.815	5.6
24.78	24.85	1358.76	VV	0.430	4	1.451	5.6
26.26	26.33	2444.45	VV	0.421	5	1.575	6
27.61	27.69	1480.33	VV	0.475	6	0.553	6.7
29.84	29.12	2690.85	VV	0.421	7	1.419	6
29.87	29.95	1831.42	VV	0.421	8	1.032	6.7
32.28	32.36	1229.82	VV	0.421	9	0.725	6.7
32.96	33.05	831.11	VV	0.421	10	0.361	7
34.76	34.85	3194.34	VB	0.64	11	1.249	7
39.18	39.31	1720.95	BP	0.421	12	0.926	7.8
45.73	45.88	218.13	PV	0.957	13	6.962E-02	8
49.17	49.33	491.53	VP	1.124	14	0.176	8

MULTIPLIER = 1

Fig 4

0.45



OVI STOP RUN

13 R.R.0638  
1260 ON CLEARED EC  
ESTD COMPENSATED ANALYSIS

RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00							
0.00							
0.00							
3.52	3.53	9.50	VV	-----	1	9.399E-02	1
7.04	7.09	7.01	VV	-----	4	9.126E-03	2
9.15	9.10	25.36	BV	0.259	5	2.032E-02	2, 3
11.50	11.61	76.95	VV	0.299	7	3.307E-02	3
12.68	12.44	30.93	VV	-----	8	3.234E-02	3
14.00	14.02	247.32	VB	0.410	9	0.260	4
15.67	15.71	89.00	BV	-----	10	6.207E-02	3, 4
16.35	16.42	82.46	VV	-----	11	4.749E-02	4
18.62	18.26	322.74	VV	-----	12	0.310	4, 5
19.03	20.04	501.56	VV	-----	13	0.419	4, 5
22.30	22.49	152.17	VV	-----	14	0.177	5
23.26	23.32	542.43	VV	-----	15	0.647	5
24.76	24.06	1041.50	VV	0.461	16	0.522	5, 6
27.50	27.60	842.59	VV	0.409	17	0.672	

MULTIPLIER = 1

RUN 40

TOTAL BASED ON AROCHLOR 1242= 3.72321

PP: GETTING CALIB 1260 PEAKS T.P. FROM DEVICE 6

PP: DONE

END 50000 SAMPLER INJECTION 0 07:15 DEC 21, 1902

SAMPLE 0 : ID CODE :

13 R.R.0638

1260 ON CLEARED EC

ESTD COMPENSATED ANALYSIS

RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00							
0.00							
0.00							
10.62	10.65	322.74	VV	-----	1	0.255	5
19.03	19.04	501.56	VV	-----	2	0.403	5
23.50	23.63	519.35	VV	-----	3	0.523	5, 6
24.76	24.78	1041.50	VV	0.461	4	1.000	5, 6
26.23	26.26	1506.34	VV	-----	5	1.039	6
27.50	27.61	842.59	VV	0.409	6	0.317	6, 7
29.01	29.04	1650.52	VV	-----	7	0.061	6
29.04	29.06	1100.52	VV	-----	8	0.603	6, 7
32.24	32.20	746.06	VV	-----	9	0.450	6, 7
32.92	32.95	525.41	VV	-----	10	0.230	7
34.72	34.74	1020.01	VV	0.624	11	0.713	7
39.12	39.14	1024.04	PP	-----	12	0.350	7, 8
45.66	45.73	132.44	PS	0.943	13	4.209E-02	8
49.09	49.10	203.42	SP	1.123	14	0.109	8

MULTIPLIER = 1

TOTAL BASED ON AROCHLOR 1260= 7.35131

BIPHENYL

AMOUNT

MONOCHLORO	9.39921E-02
DICHLORO	1.42006E-02
TRICHLORO	.101396
TETRACHLORO	.045297
PENTACHLORO	.094077
HEXACHLORO	3.29923
HEPTACHLORO	2.40704
OCTACHLORO	.429601
TOTAL IF AROCHLOR 1242=	3.72321
TOTAL IF AROCHLOR 1260=	7.35131
TOTAL BASED ON WEBB & MCCALL =	0.00564 MICROGRAMS/ML

PP: GETTING CALIB 1254 PEAKS T.P. FROM DEVICE 6

PP: DONE

END 50000 SAMPLER INJECTION 0 07:15 DEC 21, 1902

SAMPLE 0 : ID CODE :

13 R.R.0638

1260 ON CLEARED EC

ESTD COMPENSATED ANALYSIS

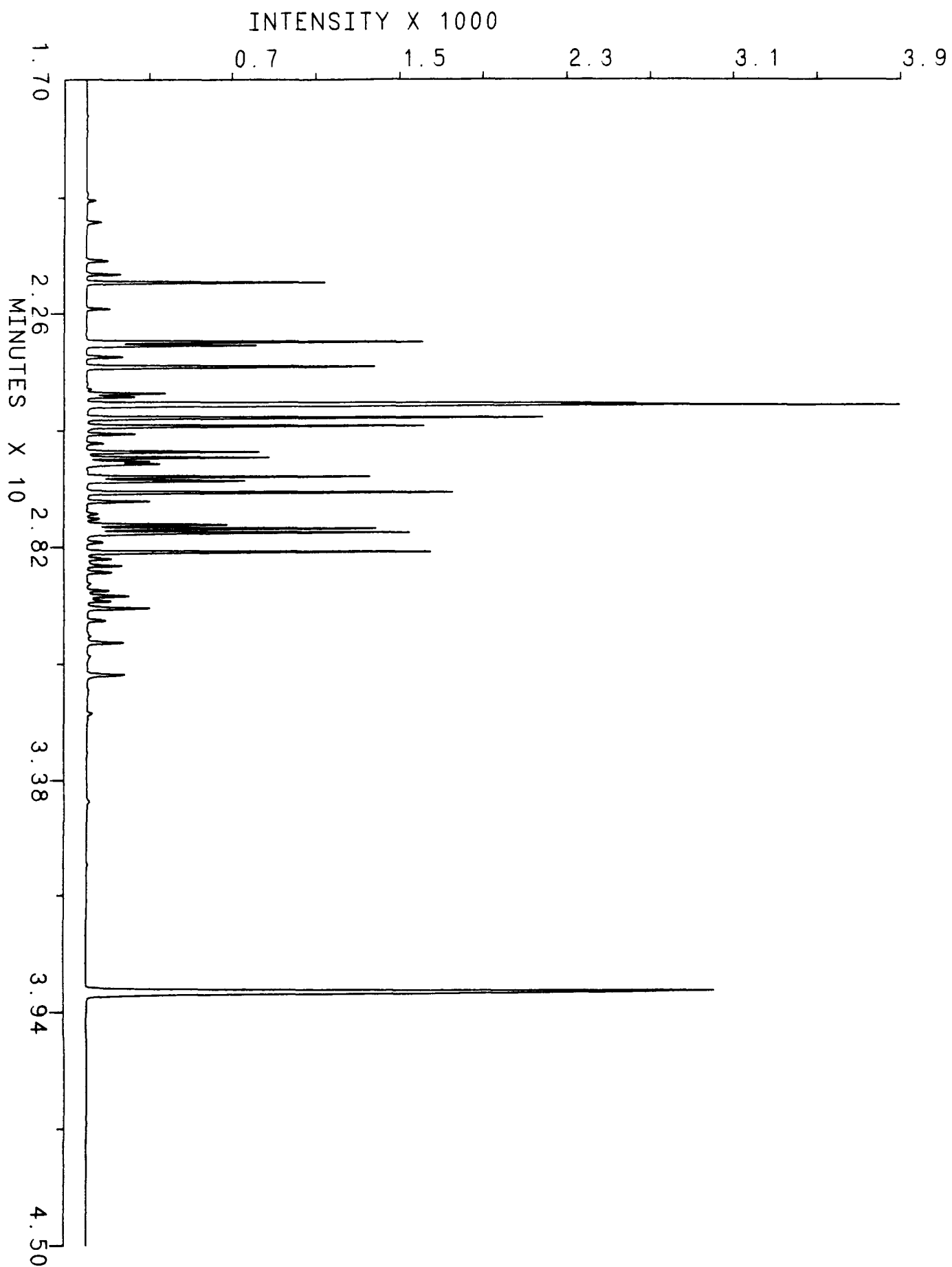
RT	EXP RT	HEIGHT	TYPE	WIDTH	CAL	AMOUNT	NAME
0.00							
0.00							
0.00							
14.00	13.90	247.32	VB	0.410	1	0.227	4
15.67	15.65	89.00	BV	-----	2	5.703E-02	4
16.35	16.40	82.46	VV	-----	3	5.025E-02	4
18.62	18.62	322.74	VV	-----	5	0.365	5
19.03	19.04	501.56	VV	-----	6	0.663	5
22.30	22.42	152.17	VV	-----	7	0.123	5
23.26	23.24	542.43	VV	-----	8	0.413	5
24.76	24.02	1041.50	VV	0.461	9	0.011	5, 6
26.23	26.23	1506.34	VV	-----	10	1.650	5, 6
27.50	27.54	842.59	VV	0.409	11	0.164E-02	6
29.01	29.03	1650.52	VV	-----	12	0.016	6
29.04	29.07	1100.52	VV	-----	13	0.020	6
32.24	31.09	746.06	VV	-----	14	0.194	7

MULTIPLIER = 1

TOTAL BASED ON AROCHLOR 1254= 6.25165

PERCENT 1242=	3.29591	.266496	PPH 1242
PERCENT 1254=	22.5630	1.02442	PPH 1254
PERCENT 1260=	74.1403	5.99472	PPH 1260

Fig. 5



4 7-23-87 GC1 STDS004, 3, 1, A1242

Fig. 6

6 7-24-87 GC1 STDS006, 3, 1, A1254

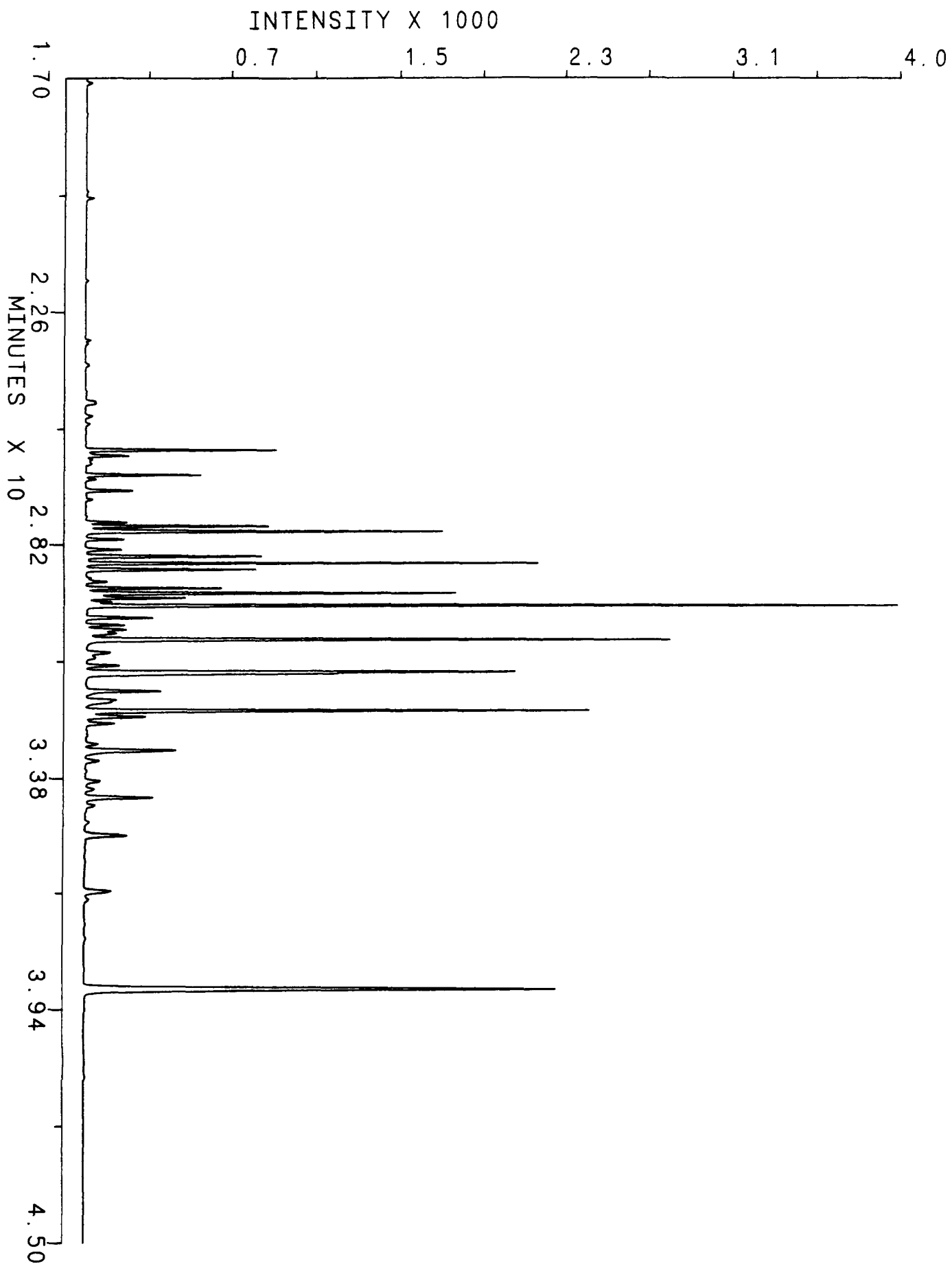
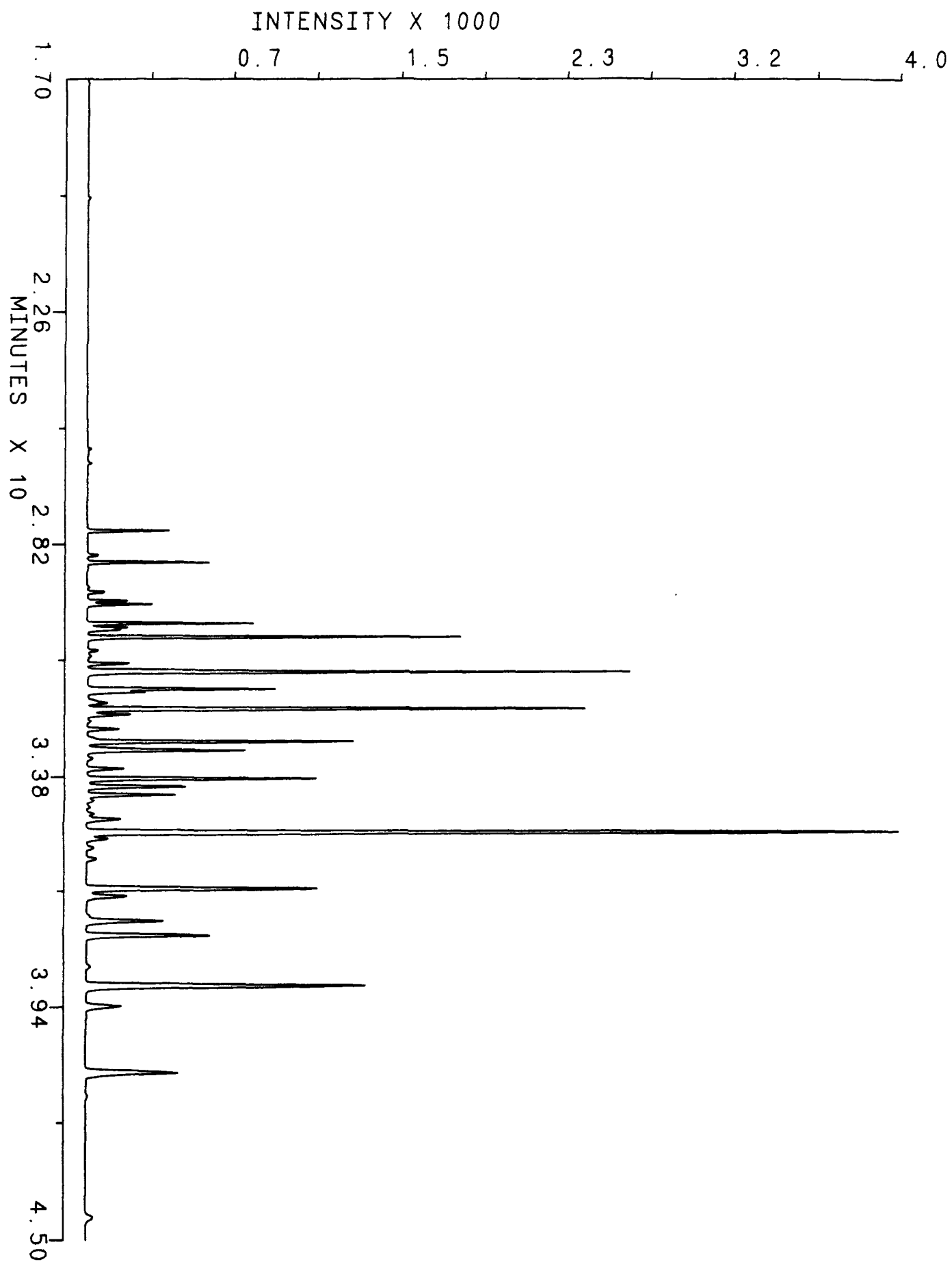




Fig. 7



7 7-24-87 GC1 STDS007, 3, 1, A1260

RET. TIME	NAME	AREA	AMT	RESPONSE FUNCTION			
				R2*(AREA^2) + R1*AREA + R0	R2	R1	R0
40.70	1	0.6	0.000000	0.00000	0.00000	0.00000	0.00000
46.74	2	0.3	0.009683	0.00000	0.00000	77.43000	0.00000
50.30	3	0.0	0.000000	0.00000	646.83002	0.00000	0.00000
50.64	4	0.0	0.000000	0.00000	131.64000	0.00000	0.00000
52.36	5	3.8	0.040948	0.00000	25.85000	0.00000	0.00000
54.80	6	5.7	0.007437	0.00000	3.13000	0.00000	0.00000
55.63	7	7.3	0.024071	0.00000	7.91000	0.00000	0.00000
56.12	8	45.7	0.104580	0.00000	5.49000	0.00000	0.00000
57.46	9	0.0	0.000000	0.00000	7.22000	0.00000	0.00000
57.73	10	5.0	0.018175	0.00000	8.72000	0.00000	0.00000
58.89	11	0.4	0.000447	0.00000	2.68000	0.00000	0.00000
59.18	12	0.0	0.000000	0.00000	48.99000	0.00000	0.00000
59.48	13	0.6	0.002904	0.00000	11.61000	0.00000	0.00000
59.79	14	67.7	0.210816	0.00000	7.47000	0.00000	0.00000
59.99	15	35.0	0.094545	0.00000	6.48000	0.00000	0.00000
60.71	16	8.8	0.014857	0.00000	4.05000	0.00000	0.00000
61.33	17	73.5	0.106319	0.00000	3.47000	0.00000	0.00000
62.08	18	0.2	0.000367	0.00000	4.40000	0.00000	0.00000
62.31	19	0.9	0.001812	0.00000	4.83000	0.00000	0.00000
62.72	20	1.3	0.001880	0.00000	3.47000	0.00000	0.00000
62.95	21	15.8	0.023184	0.00000	3.52000	0.00000	0.00000
63.16	22	9.9	0.015971	0.00000	3.87000	0.00000	0.00000
63.64	23	109.5	0.140135	0.00000	3.07000	0.00000	0.00000
63.69	24	158.9	0.165599	0.00000	2.50000	0.00000	0.00000
64.47	25	96.4	0.130201	0.00000	3.24000	0.00000	0.00000
64.98	26	69.3	0.059799	0.00000	2.07000	0.00000	0.00000
65.44	27	10.8	0.019629	0.00000	4.36000	0.00000	0.00000
65.78	28	0.0	0.000000	0.00000	7.46000	0.00000	0.00000
66.06	29	3.8	0.012815	0.00000	8.09000	0.00000	0.00000
66.37	30	0.0	0.000000	0.00000	6.34000	0.00000	0.00000
66.57	31	33.4	0.068224	0.00000	4.90000	0.00000	0.00000
66.93	32	35.1	0.053845	0.00000	3.68000	0.00000	0.00000
67.19	33	13.5	0.020428	0.00000	3.63000	0.00000	0.00000
67.32	34	16.7	0.029239	0.00000	4.20000	0.00000	0.00000
67.51	35	0.0	0.000000	0.00000	2.21000	0.00000	0.00000
67.81	36	1.0	0.002447	0.00000	5.87000	0.00000	0.00000
68.11	37	54.6	0.067599	0.00000	2.97000	0.00000	0.00000
68.37	38	48.8	0.066501	0.00000	3.91000	0.00000	0.00000
69.09	39	79.9	0.064283	0.00000	1.93000	0.00000	0.00000
69.17	40	0.0	0.000000	0.00000	2.85000	0.00000	0.00000
69.40	41	0.5	0.001065	0.00000	5.11000	0.00000	0.00000
69.63	42	13.6	0.018255	0.00000	3.22000	0.00000	0.00000
70.07	43	0.6	0.000913	0.00000	3.65000	0.00000	0.00000
70.40	44	2.9	0.004485	0.00000	3.71000	0.00000	0.00000
70.73	45	3.1	0.004252	0.00000	3.29000	0.00000	0.00000
71.07	46	30.6	0.031125	0.00000	2.44000	0.00000	0.00000
71.30	47	59.2	0.070580	0.00000	2.86000	0.00000	0.00000
71.56	48	74.3	0.074954	0.00000	2.42000	0.00000	0.00000
72.17	49	5.5	0.007681	0.00000	3.35000	0.00000	0.00000
72.76	50	77.2	0.091875	0.00000	2.83000	0.00000	0.00000
73.18	51	6.6	0.007263	0.00000	2.64000	0.00000	0.00000
73.41	52	0.7	0.000832	0.00000	2.85000	0.00000	0.00000
73.59	53	8.2	0.012989	0.00000	3.80000	0.00000	0.00000
73.97	54	5.7	0.006582	0.00000	2.77000	0.00000	0.00000
74.51	55	0.4	0.000397	0.00000	2.38000	0.00000	0.00000
74.72	56	1.2	0.002266	0.00000	4.53000	0.00000	0.00000
75.13	57	4.9	0.004739	0.00000	2.32000	0.00000	0.00000
75.46	58	10.1	0.006526	0.00000	1.55000	0.00000	0.00000
75.77	59	6.5	0.004362	0.00000	1.61000	0.00000	0.00000
76.03	60	0.0	0.000000	0.00000	3.58000	0.00000	0.00000
76.21	61	16.5	0.011280	0.00000	1.64000	0.00000	0.00000
76.68	62	0.0	0.000000	0.00000	2.81000	0.00000	0.00000
76.95	63	4.5	0.004014	0.00000	2.14000	0.00000	0.00000
77.42	64	0.2	0.000258	0.00000	3.10000	0.00000	0.00000
77.72	65	0.7	0.000694	0.00000	2.38000	0.00000	0.00000
77.79	66	0.0	0.000000	0.00000	1.89000	0.00000	0.00000
77.93	67	1.2	0.001296	0.00000	2.59000	0.00000	0.00000
78.15	68	0.0	0.000000	0.00000	2.41000	0.00000	0.00000
78.34	69	10.3	0.008716	0.00000	2.83000	0.00000	0.00000
78.45	70	0.0	0.000000	0.00000	2.29000	0.00000	0.00000
79.19	71	1.4	0.001494	0.00000	2.56000	0.00000	0.00000
79.34	72	0.3	0.000231	0.00000	1.85000	0.00000	0.00000
79.91	73	0.1	0.000117	0.00000	2.80000	0.00000	0.00000
80.29	74	11.7	0.005316	0.00000	1.09000	0.00000	0.00000
80.44	75	0.0	0.000000	0.00000	3.32000	0.00000	0.00000
81.27	76	0.8	0.000477	0.00000	1.43000	0.00000	0.00000
81.47	77	0.6	0.000280	0.00000	1.12000	0.00000	0.00000
81.65	78	0.0	0.000000	0.00000	3.43000	0.00000	0.00000
82.04	79	0.2	0.000190	0.00000	2.28000	0.00000	0.00000
82.17	80	0.2	0.000228	0.00000	2.74000	0.00000	0.00000
82.31	81	0.0	0.000000	0.00000	1.13000	0.00000	0.00000
82.71	82	2.0	0.001359	0.00000	1.63000	0.00000	0.00000
83.07	83	0.4	0.000283	0.00000	1.70000	0.00000	0.00000
83.45	84	0.2	0.000193	0.00000	2.31000	0.00000	0.00000
83.93	85	0.0	0.000000	0.00000	2.17000	0.00000	0.00000
84.29	86	0.0	0.000000	0.00000	1.15000	0.00000	0.00000
84.50	87	0.0	0.000000	0.00000	3.15000	0.00000	0.00000
84.73	88	0.0	0.000000	0.00000	1.88000	0.00000	0.00000
85.15	89	0.7	0.000371	0.00000	1.27000	0.00000	0.00000
85.27	90	0.0	0.000000	0.00000	1.60000	0.00000	0.00000
85.76	91	0.0	0.000000	0.00000	3.76000	0.00000	0.00000
86.40	92	0.0	0.000000	0.00000	1.47000	0.00000	0.00000
87.20	93	0.3	0.000181	0.00000	1.45000	0.00000	0.00000
87.51	94	0.0	0.000000	0.00000	1.89000	0.00000	0.00000
88.13	95	1.4	0.000928	0.00000	1.59000	0.00000	0.00000
88.38	96	0.0	0.000000	0.00000	1.03000	0.00000	0.00000
88.49	97	0.0	0.000000	0.00000	1.80000	0.00000	0.00000
88.87	98	0.0	0.000000	0.00000	0.59000	0.00000	0.00000
89.31	99	0.0	0.000000	0.00000	1.74000	0.00000	0.00000
89.64	100	0.0	0.000000	0.00000	1.88000	0.00000	0.00000
90.16	101	0.0	0.000000	0.00000	1.26000	0.00000	0.00000
90.47	102	8.2	0.000895	0.00000	1.14000	0.00000	0.00000
90.85	103	0.0	0.000000	0.00000	0.85000	0.00000	0.00000
91.39	104	0.0	0.000000	0.00000	0.81000	0.00000	0.00000
92.14	105	0.8	0.000347	0.00000	1.04000	0.00000	0.00000
93.93	106	0.0	0.000000	0.00000	1.14000	0.00000	0.00000
94.40	107	0.0	0.000000	0.00000	1.40000	0.00000	0.00000
95.63	108	0.0	0.000000	0.00000	1.12000	0.00000	0.00000
95.96	109	0.0	0.000000	0.00000	1.53000	0.00000	0.00000
96.86	110	0.0	0.000000	0.00000	1.22000	0.00000	0.00000
98.77	111	0.0	0.000000	0.00000	0.80000	0.00000	0.00000
100.00	1.3.	265.1	INT.STD.	0.00000	1.00000	0.00000	0.00000
101.23	112	0.0	0.000000	0.00000	1.42000	0.00000	0.00000
101.85	113	0.0	0.000000	0.00000	1.02000	0.00000	0.00000
103.26	114	0.0	0.000000	0.00000	0.91000	0.00000	0.00000
105.42	115	0.0	0.000000	0.00000	1.07000	0.00000	0.00000
106.79	116	0.0	0.000000	0.00000	0.85000	0.00000	0.00000
114.24	117	0.0	0.000000	0.00000	2.97000	0.00000	0.00000
122.90	118	0.0	0.000000	0.00000	1.19000	0.00000	0.00000

AMT TOTAL = 1.967442

RET. TIME	NAME	AREA	AMT	RESPONSE FUNCTION		
				R2*(AREA^2) + R1*AREA + R0	R2	R1
40.69	1	2.2	0.000000	0.00000	0.00000	0.00000
46.74	2	0.0	0.000000	0.00000	0.00000	0.00000
50.30	3	0.0	0.000000	0.00000	0.00000	0.00000
50.64	4	0.0	0.000000	0.00000	0.00000	0.00000
52.36	5	0.0	0.000000	0.00000	0.00000	0.00000
54.80	6	0.0	0.000000	0.00000	0.00000	0.00000
55.60	7	0.1	0.000487	0.00000	0.00000	0.00000
56.12	8	0.8	0.002703	0.00000	0.00000	0.00000
57.46	9	0.0	0.000000	0.00000	0.00000	0.00000
57.76	10	0.1	0.000537	0.00000	0.00000	0.00000
58.78	11	0.0	0.000000	0.00000	0.00000	0.00000
59.18	12	0.0	0.000000	0.00000	0.00000	0.00000
59.48	13	0.0	0.000000	0.00000	0.00000	0.00000
59.82	14	1.3	0.005976	0.00000	0.00000	0.00000
60.03	15	0.7	0.002792	0.00000	0.00000	0.00000
60.69	16	0.2	0.000498	0.00000	0.00000	0.00000
61.31	17	1.5	0.003203	0.00000	0.00000	0.00000
62.13	18	0.0	0.000000	0.00000	0.00000	0.00000
62.42	19	0.2	0.000594	0.00000	0.00000	0.00000
62.73	20	0.0	0.000000	0.00000	0.00000	0.00000
62.98	21	0.5	0.001083	0.00000	0.00000	0.00000
63.16	22	0.0	0.000000	0.00000	0.00000	0.00000
63.60	23	2.8	0.005290	0.00000	0.00000	0.00000
63.70	24	2.5	0.003846	0.00000	0.00000	0.00000
64.52	25	2.4	0.004786	0.00000	0.00000	0.00000
64.99	26	1.4	0.001783	0.00000	0.00000	0.00000
65.48	27	0.5	0.001342	0.00000	0.00000	0.00000
65.78	28	0.0	0.000000	0.00000	0.00000	0.00000
66.04	29	0.2	0.000996	0.00000	0.00000	0.00000
66.37	30	0.0	0.000000	0.00000	0.00000	0.00000
66.58	31	37.7	0.113687	0.00000	0.00000	0.00000
66.94	32	10.8	0.024459	0.00000	0.00000	0.00000
67.20	33	1.7	0.003798	0.00000	0.00000	0.00000
67.33	34	0.9	0.002326	0.00000	0.00000	0.00000
67.46	35	1.6	0.002176	0.00000	0.00000	0.00000
67.78	36	0.0	0.000000	0.00000	0.00000	0.00000
68.12	37	23.5	0.042953	0.00000	0.00000	0.00000
68.41	38	2.5	0.006016	0.00000	0.00000	0.00000
69.10	39	11.5	0.013659	0.00000	0.00000	0.00000
69.17	40	0.0	0.000000	0.00000	0.00000	0.00000
69.46	41	0.5	0.001572	0.00000	0.00000	0.00000
69.67	42	1.9	0.003765	0.00000	0.00000	0.00000
70.00	43	0.4	0.000899	0.00000	0.00000	0.00000
70.46	44	0.2	0.000457	0.00000	0.00000	0.00000
70.75	45	0.6	0.001215	0.00000	0.00000	0.00000
71.00	46	9.1	0.013665	0.00000	0.00000	0.00000
71.34	47	39.6	0.069700	0.00000	0.00000	0.00000
71.67	48	84.3	0.125550	0.00000	0.00000	0.00000
72.16	49	9.4	0.019380	0.00000	0.00000	0.00000
72.70	50	9.0	0.015675	0.00000	0.00000	0.00000
73.19	51	42.5	0.069050	0.00000	0.00000	0.00000
73.42	52	0.5	0.000877	0.00000	0.00000	0.00000
73.62	53	93.8	0.219361	0.00000	0.00000	0.00000
74.01	54	34.5	0.058813	0.00000	0.00000	0.00000
74.55	55	1.7	0.002490	0.00000	0.00000	0.00000
74.76	56	5.3	0.014776	0.00000	0.00000	0.00000
75.17	57	29.7	0.042405	0.00000	0.00000	0.00000
75.40	58	82.4	0.078602	0.00000	0.00000	0.00000
75.78	59	24.3	0.024077	0.00000	0.00000	0.00000
76.02	60	5.9	0.012999	0.00000	0.00000	0.00000
76.25	61	171.0	0.172589	0.00000	0.00000	0.00000
76.68	62	0.9	0.001556	0.00000	0.00000	0.00000
76.99	63	14.7	0.019360	0.00000	0.00000	0.00000
77.43	64	9.0	0.017170	0.00000	0.00000	0.00000
77.71	65	14.1	0.020652	0.00000	0.00000	0.00000
77.79	66	0.0	0.000000	0.00000	0.00000	0.00000
77.94	67	8.8	0.014027	0.00000	0.00000	0.00000
78.15	68	0.0	0.000000	0.00000	0.00000	0.00000
78.35	69	161.5	0.201763	0.00000	0.00000	0.00000
78.77	70	0.3	0.000423	0.00000	0.00000	0.00000
79.13	71	9.5	0.014967	0.00000	0.00000	0.00000
79.46	72	4.4	0.005237	0.00000	0.00000	0.00000
79.95	73	9.0	0.015509	0.00000	0.00000	0.00000
80.33	74	113.8	0.076338	0.00000	0.00000	0.00000
80.44	75	53.1	0.108494	0.00000	0.00000	0.00000
81.26	76	0.9	0.000732	0.00000	0.00000	0.00000
81.52	77	21.0	0.015026	0.00000	0.00000	0.00000
81.65	78	0.0	0.000000	0.00000	0.00000	0.00000
82.00	79	0.9	0.012400	0.00000	0.00000	0.00000
82.19	80	7.8	0.013153	0.00000	0.00000	0.00000
82.31	81	0.0	0.000000	0.00000	0.00000	0.00000
82.72	82	136.4	0.136820	0.00000	0.00000	0.00000
83.00	83	17.6	0.010413	0.00000	0.00000	0.00000
83.50	84	8.6	0.012226	0.00000	0.00000	0.00000
83.90	85	1.3	0.001736	0.00000	0.00000	0.00000
84.29	86	0.0	0.000000	0.00000	0.00000	0.00000
84.50	87	0.0	0.000000	0.00000	0.00000	0.00000
84.76	88	4.2	0.004059	0.00000	0.00000	0.00000
85.17	89	32.6	0.025400	0.00000	0.00000	0.00000
85.27	90	0.0	0.000000	0.00000	0.00000	0.00000
85.01	91	5.3	0.012264	0.00000	0.00000	0.00000
86.43	92	0.0	0.000724	0.00000	0.00000	0.00000
87.04	93	6.1	0.005443	0.00000	0.00000	0.00000
87.56	94	3.5	0.004071	0.00000	0.00000	0.00000
88.07	95	23.2	0.022702	0.00000	0.00000	0.00000
88.30	96	0.0	0.000000	0.00000	0.00000	0.00000
88.56	97	4.2	0.002585	0.00000	0.00000	0.00000
88.87	98	0.6	0.000218	0.00000	0.00000	0.00000
89.31	99	0.0	0.000000	0.00000	0.00000	0.00000
89.72	100	1.0	0.001157	0.00000	0.00000	0.00000
90.16	101	0.0	0.000000	0.00000	0.00000	0.00000
90.51	102	15.6	0.010945	0.00000	0.00000	0.00000
91.00	103	0.2	0.000105	0.00000	0.00000	0.00000
91.44	104	0.6	0.000299	0.00000	0.00000	0.00000
92.13	105	0.8	0.000512	0.00000	0.00000	0.00000
93.90	106	11.6	0.008138	0.00000	0.00000	0.00000
94.47	107	2.4	0.002068	0.00000	0.00000	0.00000
95.68	108	0.3	0.000207	0.00000	0.00000	0.00000
96.02	109	0.9	0.000847	0.00000	0.00000	0.00000
96.86	110	1.0	0.000751	0.00000	0.00000	0.00000
98.84	111	0.3	0.000148	0.00000	0.00000	0.00000
100.00	1.8	190.5	INT. STD.	0.00000	0.00000	0.00000
101.34	112	0.4	0.000350	0.00000	0.00000	0.00000
101.85	113	0.0	0.000000	0.00000	0.00000	0.00000
103.26	114	0.0	0.000000	0.00000	0.00000	0.00000
105.50	115	0.8	0.000527	0.00000	0.00000	0.00000
106.79	116	0.0	0.000000	0.00000	0.00000	0.00000
114.24	117	0.0	0.000000	0.00000	0.00000	0.00000
122.90	118	0.0	0.000000	0.00000	0.00000	0.00000

AMT TOTAL = 2.003465

RET. TIME	NAME	AREA	AMT	RESPONSE FUNCTION			
				R2*(AREA^2) + R1*AREA + R0	R2	R1	R0
40.69	1	1.1	0.000000	0.000000	0.000000	0.000000	0.000000
46.74	2	0.0	0.000000	0.000000	0.000000	77.430000	0.000000
50.30	3	0.0	0.000000	0.000000	0.000000	646.830020	0.000000
50.62	4	0.0	0.000000	0.000000	0.000000	131.640000	0.000000
52.36	5	0.0	0.000000	0.000000	0.000000	25.850000	0.000000
54.80	6	0.0	0.000000	0.000000	0.000000	3.130000	0.000000
55.63	7	0.0	0.000000	0.000000	0.000000	7.910000	0.000000
56.12	8	0.0	0.000000	0.000000	0.000000	5.490000	0.000000
57.46	9	0.0	0.000000	0.000000	0.000000	7.220000	0.000000
57.73	10	0.0	0.000000	0.000000	0.000000	8.720000	0.000000
58.78	11	0.0	0.000000	0.000000	0.000000	2.680000	0.000000
59.18	12	0.0	0.000000	0.000000	0.000000	48.990000	0.000000
59.48	13	0.0	0.000000	0.000000	0.000000	11.610000	0.000000
59.79	14	0.0	0.000000	0.000000	0.000000	7.470000	0.000000
59.99	15	0.0	0.000000	0.000000	0.000000	6.480000	0.000000
60.71	16	0.0	0.000000	0.000000	0.000000	4.050000	0.000000
61.33	17	0.0	0.000000	0.000000	0.000000	3.470000	0.000000
62.13	18	0.0	0.000000	0.000000	0.000000	4.400000	0.000000
62.38	19	0.0	0.000000	0.000000	0.000000	4.830000	0.000000
62.73	20	0.0	0.000000	0.000000	0.000000	3.470000	0.000000
62.95	21	0.0	0.000000	0.000000	0.000000	3.520000	0.000000
63.16	22	0.0	0.000000	0.000000	0.000000	3.870000	0.000000
63.64	23	0.0	0.000000	0.000000	0.000000	3.070000	0.000000
63.69	24	0.0	0.000000	0.000000	0.000000	2.500000	0.000000
64.47	25	0.0	0.000000	0.000000	0.000000	3.240000	0.000000
65.14	26	0.2	0.000300	0.000000	0.000000	2.070000	0.000000
65.44	27	0.0	0.000000	0.000000	0.000000	4.360000	0.000000
65.78	28	0.0	0.000000	0.000000	0.000000	7.460000	0.000000
66.06	29	0.0	0.000000	0.000000	0.000000	8.090000	0.000000
66.37	30	0.0	0.000000	0.000000	0.000000	6.340000	0.000000
66.56	31	1.2	0.004267	0.000000	0.000000	4.900000	0.000000
66.92	32	0.1	0.000267	0.000000	0.000000	3.680000	0.000000
67.19	33	0.0	0.000000	0.000000	0.000000	3.630000	0.000000
67.32	34	0.0	0.000000	0.000000	0.000000	4.200000	0.000000
67.43	35	1.2	0.001925	0.000000	0.000000	2.210000	0.000000
67.78	36	0.0	0.000000	0.000000	0.000000	5.870000	0.000000
68.10	37	0.4	0.000062	0.000000	0.000000	2.970000	0.000000
68.37	38	0.0	0.000000	0.000000	0.000000	3.910000	0.000000
69.05	39	0.3	0.000420	0.000000	0.000000	1.930000	0.000000
69.17	40	0.0	0.000000	0.000000	0.000000	2.850000	0.000000
69.41	41	0.2	0.000742	0.000000	0.000000	5.110000	0.000000
69.63	42	0.0	0.000000	0.000000	0.000000	3.220000	0.000000
70.07	43	0.0	0.000000	0.000000	0.000000	3.650000	0.000000
70.40	44	0.0	0.000000	0.000000	0.000000	3.710000	0.000000
70.73	45	0.0	0.000000	0.000000	0.000000	3.290000	0.000000
71.05	46	0.2	0.000354	0.000000	0.000000	2.440000	0.000000
71.29	47	0.6	0.001245	0.000000	0.000000	2.860000	0.000000
71.65	48	17.6	0.030910	0.000000	0.000000	2.420000	0.000000
72.11	49	0.2	0.000406	0.000000	0.000000	3.350000	0.000000
72.75	50	0.1	0.000205	0.000000	0.000000	2.830000	0.000000
73.16	51	3.2	0.006131	0.000000	0.000000	2.640000	0.000000
73.40	52	0.0	0.000000	0.000000	0.000000	2.850000	0.000000
73.60	53	24.1	0.066462	0.000000	0.000000	3.800000	0.000000
73.90	54	0.6	0.001206	0.000000	0.000000	2.770000	0.000000
74.55	55	0.0	0.000000	0.000000	0.000000	2.380000	0.000000
74.73	56	0.0	0.000000	0.000000	0.000000	4.530000	0.000000
75.12	57	0.9	0.001515	0.000000	0.000000	2.320000	0.000000
75.45	58	4.5	0.005062	0.000000	0.000000	1.550000	0.000000
75.73	59	0.4	0.000467	0.000000	0.000000	1.610000	0.000000
75.99	60	9.3	0.024162	0.000000	0.000000	3.580000	0.000000
76.20	61	14.0	0.016663	0.000000	0.000000	1.640000	0.000000
76.68	62	0.0	0.000000	0.000000	0.000000	2.810000	0.000000
76.94	63	0.2	0.000311	0.000000	0.000000	2.140000	0.000000
77.40	64	33.4	0.075142	0.000000	0.000000	3.100000	0.000000
77.66	65	8.7	0.015827	0.000000	0.000000	2.380000	0.000000
77.79	66	8.3	0.011384	0.000000	0.000000	1.890000	0.000000
77.91	67	0.0	0.000000	0.000000	0.000000	2.590000	0.000000
78.15	68	0.0	0.000000	0.000000	0.000000	2.410000	0.000000
78.25	69	87.6	0.129055	0.000000	0.000000	2.030000	0.000000
78.45	70	0.0	0.000000	0.000000	0.000000	2.290000	0.000000
79.10	71	3.1	0.005759	0.000000	0.000000	2.560000	0.000000
79.41	72	1.5	0.002014	0.000000	0.000000	1.850000	0.000000
79.90	73	10.7	0.021743	0.000000	0.000000	2.800000	0.000000
80.28	74	0.0	0.000000	0.000000	0.000000	1.090000	0.000000
80.44	75	154.3	0.371773	0.000000	0.000000	3.320000	0.000000
81.25	76	0.0	0.000000	0.000000	0.000000	1.430000	0.000000
81.49	77	47.2	0.038365	0.000000	0.000000	1.120000	0.000000
81.65	78	14.2	0.035347	0.000000	0.000000	3.430000	0.000000
82.05	79	0.0	0.000000	0.000000	0.000000	2.280000	0.000000
82.16	80	0.0	0.000000	0.000000	0.000000	2.740000	0.000000
82.31	81	8.8	0.007217	0.000000	0.000000	1.130000	0.000000
82.72	82	150.7	0.178269	0.000000	0.000000	1.630000	0.000000
83.03	83	12.2	0.015852	0.000000	0.000000	1.780000	0.000000
83.42	84	1.7	0.002850	0.000000	0.000000	2.310000	0.000000
83.93	85	9.3	0.014646	0.000000	0.000000	2.170000	0.000000
84.22	86	0.1	0.000083	0.000000	0.000000	1.150000	0.000000
84.50	87	2.2	0.005029	0.000000	0.000000	3.150000	0.000000
84.73	88	72.2	0.098507	0.000000	0.000000	1.880000	0.000000
85.10	89	0.0	0.000000	0.000000	0.000000	1.270000	0.000000
85.27	90	48.4	0.056200	0.000000	0.000000	1.680000	0.000000
85.76	91	2.6	0.007895	0.000000	0.000000	3.760000	0.000000
86.40	92	11.5	0.012268	0.000000	0.000000	1.470000	0.000000
86.89	93	69.4	0.073830	0.000000	0.000000	1.450000	0.000000
87.51	94	32.4	0.044441	0.000000	0.000000	1.890000	0.000000
88.05	95	26.8	0.030925	0.000000	0.000000	1.590000	0.000000
88.38	96	3.3	0.002467	0.000000	0.000000	1.030000	0.000000
88.49	97	0.0	0.000000	0.000000	0.000000	1.080000	0.000000
88.87	98	1.8	0.000771	0.000000	0.000000	0.590000	0.000000
89.31	99	2.9	0.003462	0.000000	0.000000	1.740000	0.000000
89.64	100	12.0	0.016372	0.000000	0.000000	1.880000	0.000000
90.16	101	0.0	0.000000	0.000000	0.000000	1.260000	0.000000
90.44	102	284.8	0.235624	0.000000	0.000000	1.140000	0.000000
90.85	103	8.5	0.005243	0.000000	0.000000	0.850000	0.000000
91.39	104	3.4	0.001999	0.000000	0.000000	0.810000	0.000000
92.06	105	4.6	0.003472	0.000000	0.000000	1.040000	0.000000
93.93	106	88.6	0.073301	0.000000	0.000000	1.140000	0.000000
94.40	107	17.4	0.017679	0.000000	0.000000	1.480000	0.000000
95.63	108	0.0	0.000000	0.000000	0.000000	1.120000	0.000000
95.96	109	32.0	0.035532	0.000000	0.000000	1.530000	0.000000
96.06	110	50.3	0.044535	0.000000	0.000000	1.220000	0.000000
96.77	111	2.7	0.001568	0.000000	0.000000	0.800000	0.000000
100.00	112	123.6	INT. STD.	0.000000	0.000000	1.000000	0.000000
101.23	113	16.9	0.017416	0.000000	0.000000	1.420000	0.000000
101.85	114	0.9	0.000666	0.000000	0.000000	1.020000	0.000000
103.26	115	0.8	0.000528	0.000000	0.000000	0.910000	0.000000
105.42	116	45.3	0.035177	0.000000	0.000000	1.070000	0.000000
106.79	117	1.8	0.001110	0.000000	0.000000	0.850000	0.000000
114.24	118	6.5	0.014010	0.000000	0.000000	2.970000	0.000000
122.90	119	0.0	0.000000	0.000000	0.000000	1.190000	0.000000

AMT TOTAL = 1.926318

— 438 —

24